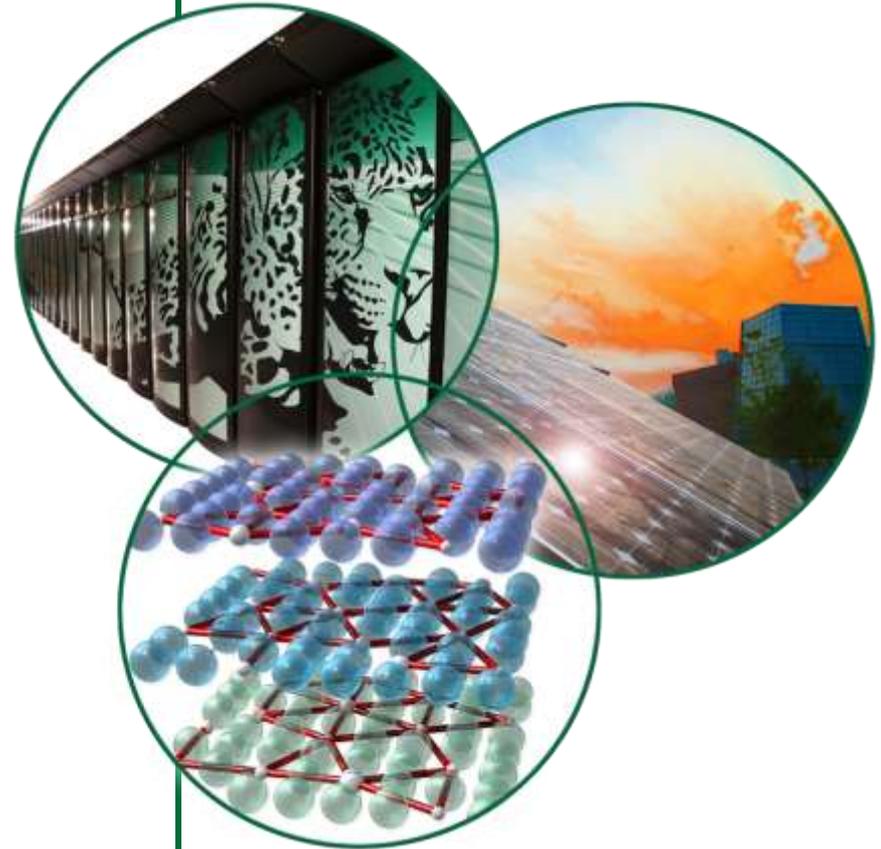


Linac Modulator Upgrades

David E. Anderson



Outline

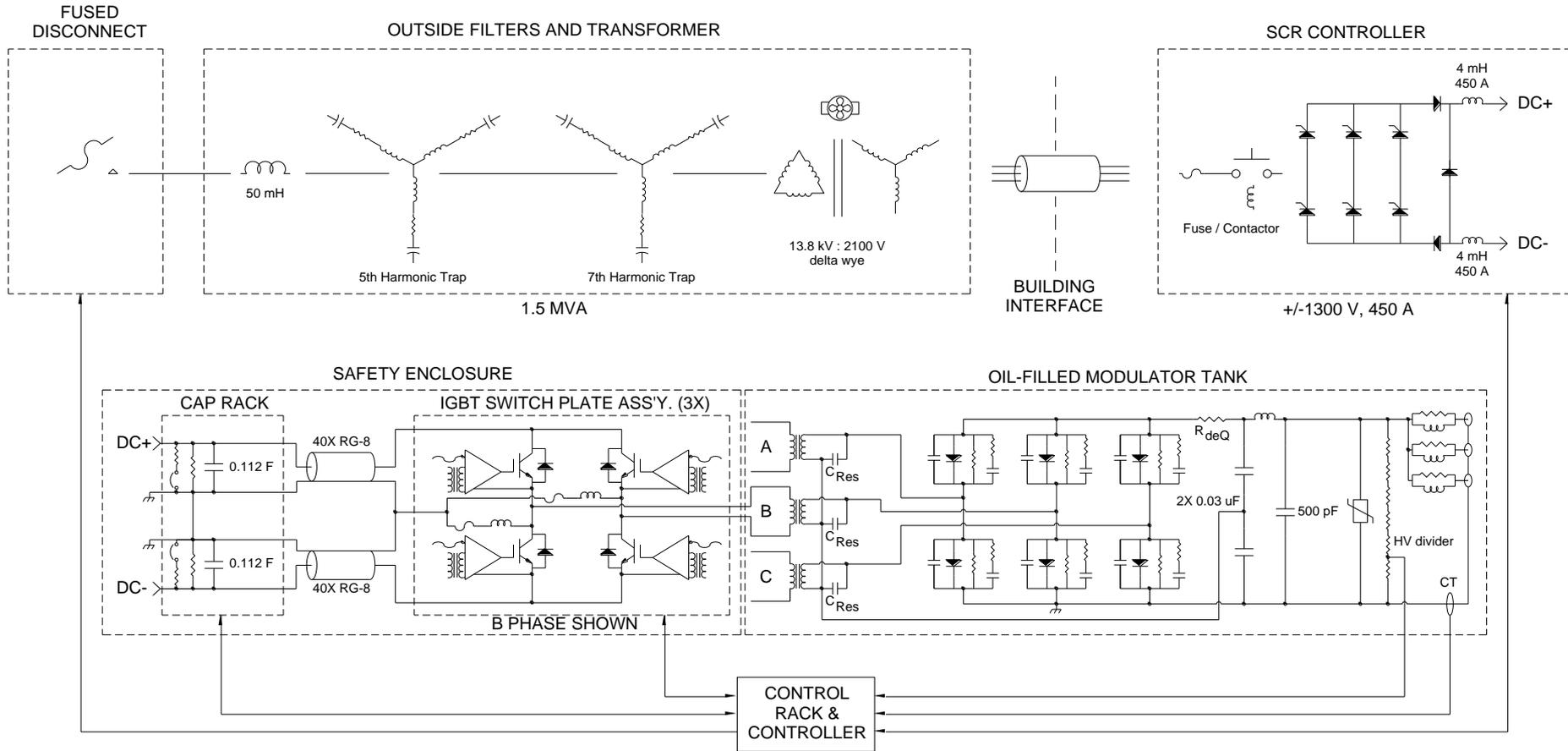
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High Level Operating Parameters

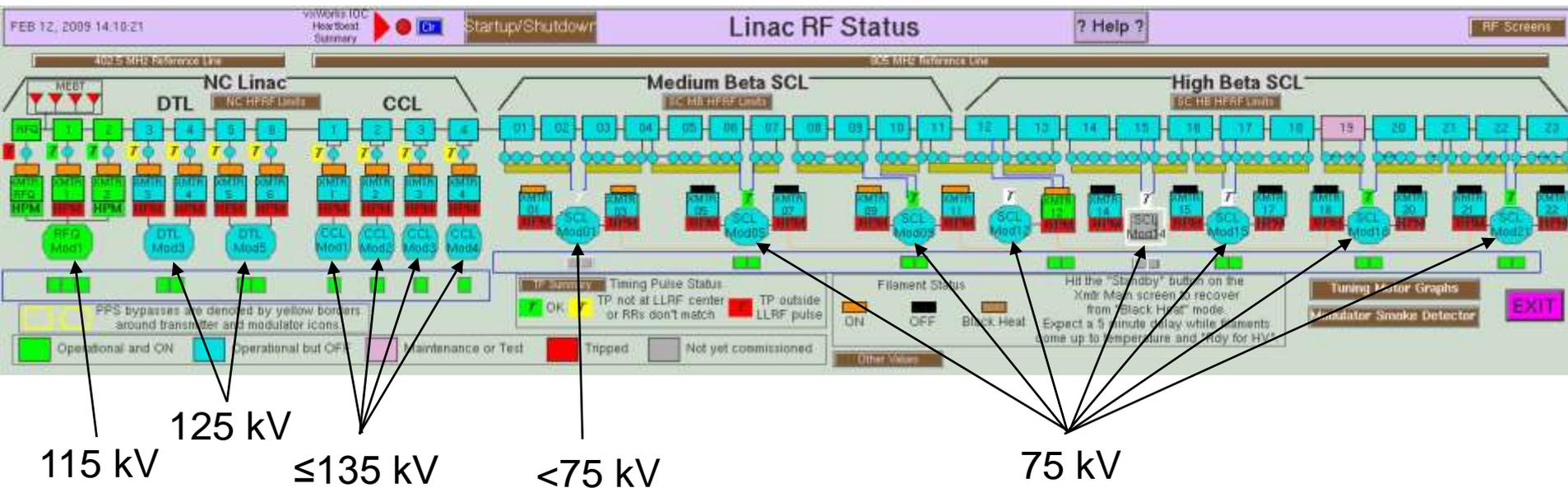
- Input line voltage: 13.8 kV, 60 Hz
- Pulsed output voltage: $\leq 140 \text{ kV}^1$
- Peak output current: $\leq 130 \text{ A}^1$
- Peak power: 11 MW
- Rated Average power: 1 MW
- Maximum pulse width: 1.35 ms
- Maximum pulse repetition frequency: 60 Hz
- IGBT switching frequency: 20 kHz
- Maximum IGBT bus voltage: 1300 V

¹depending on klystron load and location of HVCM system, SCL systems typically run at 75 kV

HVCM Simplified Block Diagram



Cavity / Klystron / Modulator Layout



- Multiple HVCM/Klystron Configurations
- Peak Power 11 MW, Average Power 1 MW design

Upgrade Overview

- Initial focus was on the SCR Controller – brought in manufacturer but little help
- Several SCR upgrades implemented based on failure analysis and observed behavior – rapid improvement resulted
- Early modulator upgrades focused on magnetics & other in-tank components
- Switchplate fires followed quickly, shifted to caps, IGBTs and Safety Enclosure internal construction materials
- Implemented fire mitigation and extinguishing systems, fire response rate improved
- With recommendations from review committees, IGBT improvements and analysis of operational statistics, focus has shifted to power electronics, controller and component derating

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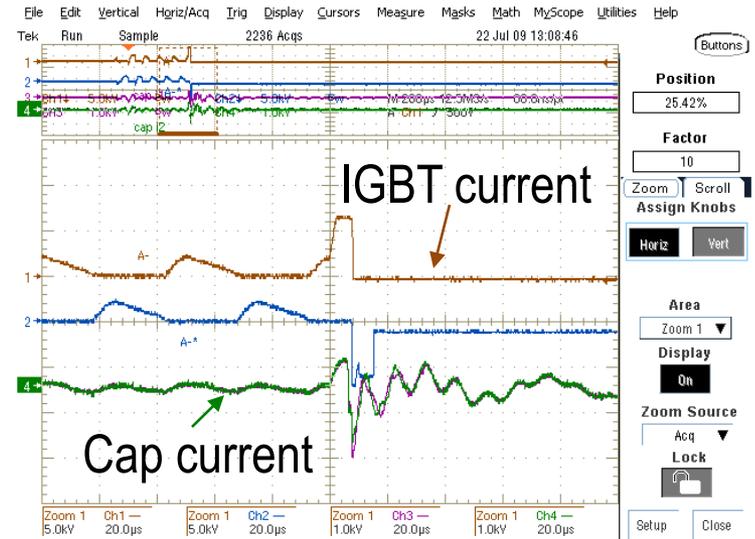
HVCM Modulator Upgrades AIP-02

- Higher duty cycle revealed system limitations, SCL IGBT commutation current issues
 - Retuned SCL resonant circuit parameters
 - Installed new magnetics
 - Installed Dynamic Fault Detection Chassis (DFDC)
 - Protects transformer saturation
 - Protects from dV/dt events
- New Rogowski probes show I_C
- Real time signal monitoring

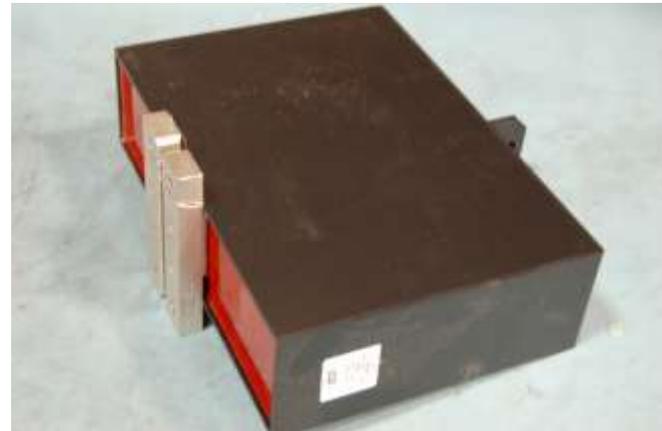


HVCM Fires – Capacitor Replacement

- Cause of multiple fires, other failures from collateral damage
- Replacing capacitors w/ self-healing AVX units shown
 - 500 fault shots + ~1 year of ops on 12 units and largest $\Delta C \approx 0.2\%$



- Self-clearing = no catastrophic failures, no collateral damage



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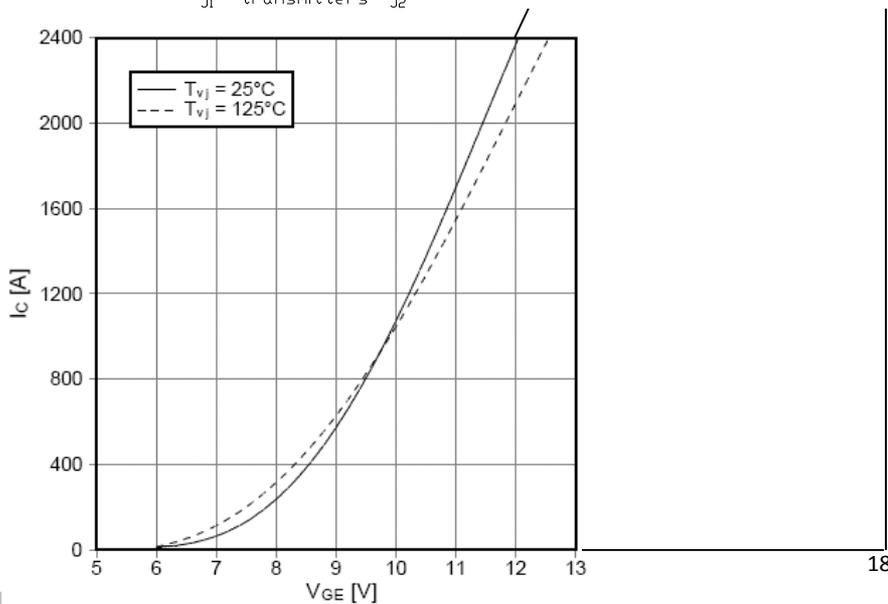
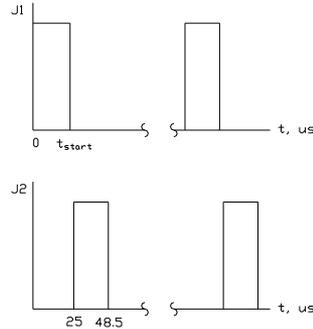
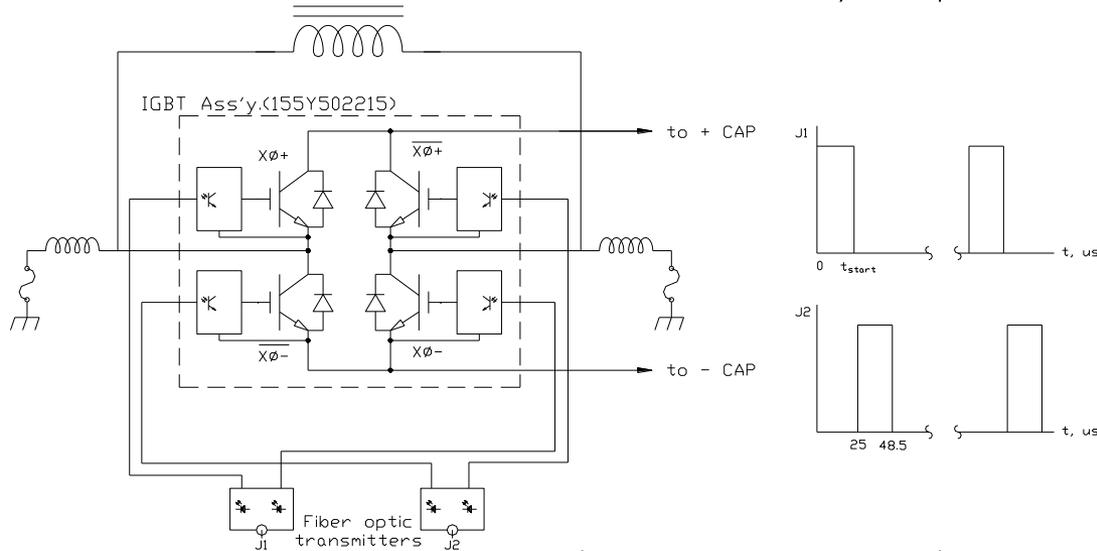
HVCM Development Resources

- Dedicated project under Neutron Facilities Development Division effective October 2008
- 3 engineers, 1 new position
 - David Anderson, Team Lead, System Engineer
 - Dennis Solley, specialization in Power Electronics
 - Mark Wezensky, specialization in Control of Electronic Systems
- 2-3 matrixed technicians
 - 1 operating test stand, 1 developing electronic systems, 1 PCB designer
- Help from SLAC team



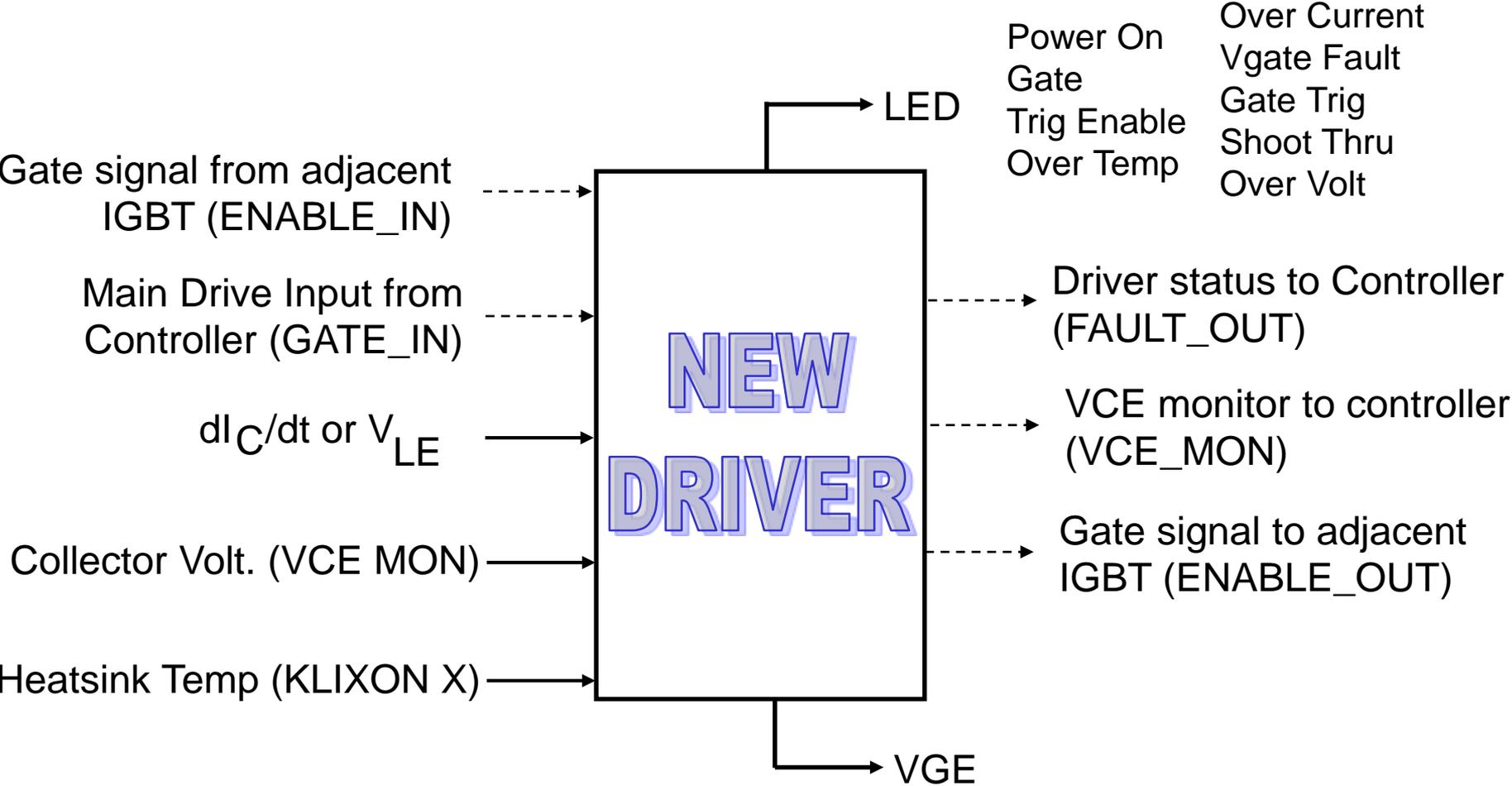
- HEBT Beamstick Load Test Stand
 - Emulates SCL modulator
 - Dedicated to HVCM Development
- RFTF available (DTL/CCL)
- Installing SLAC Single Phase Test Stand

HVCM Existing IGBT Gate Drive Concerns



- Severe overdrive increased saturated current levels
 - Fault currents higher
 - Carrier recombination time longer?
- Slow drift of electronic delays
 - Leads to timing skew
 - Leads to flux saturation
- No on-board IGBT fault detection / protection
- 120 V ac distribution safety concerns
- Insufficient isolation derating for operating voltages
- Poor EMI shielding
- Interface w/ new controller

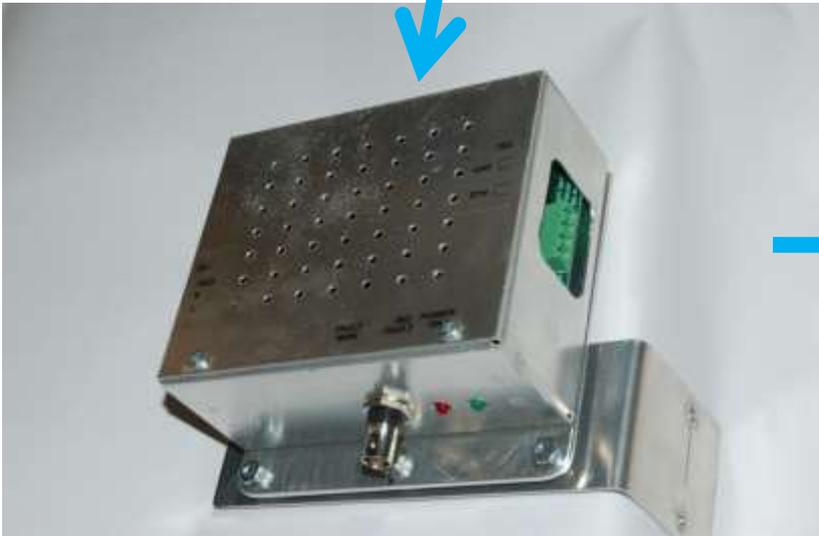
New Gate Driver Improvements



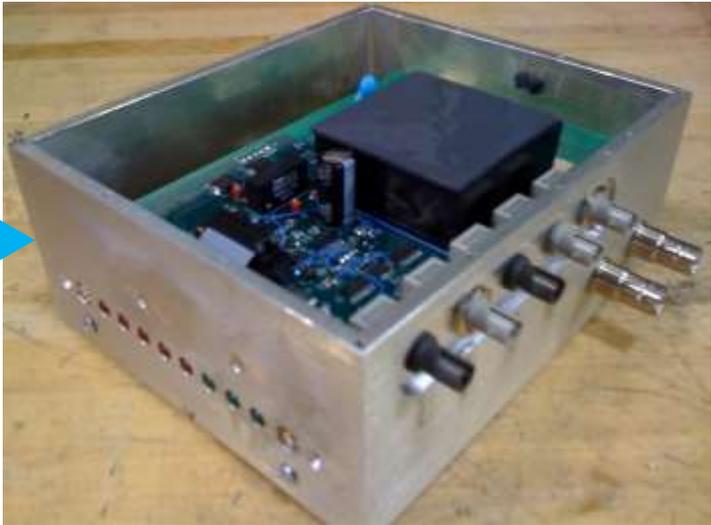
IGBT New Gate Drive Card Evolution



Original LANL Driver

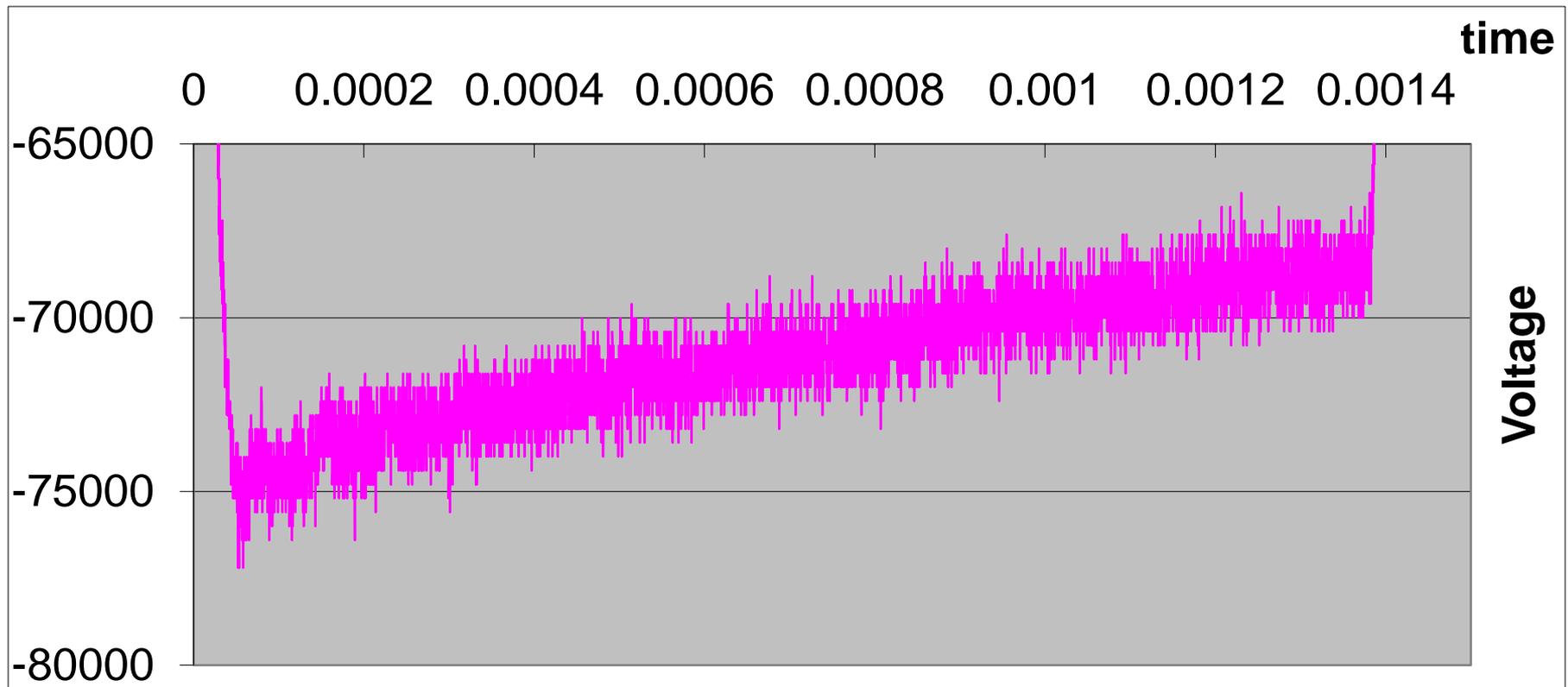


Original SLAC Driver



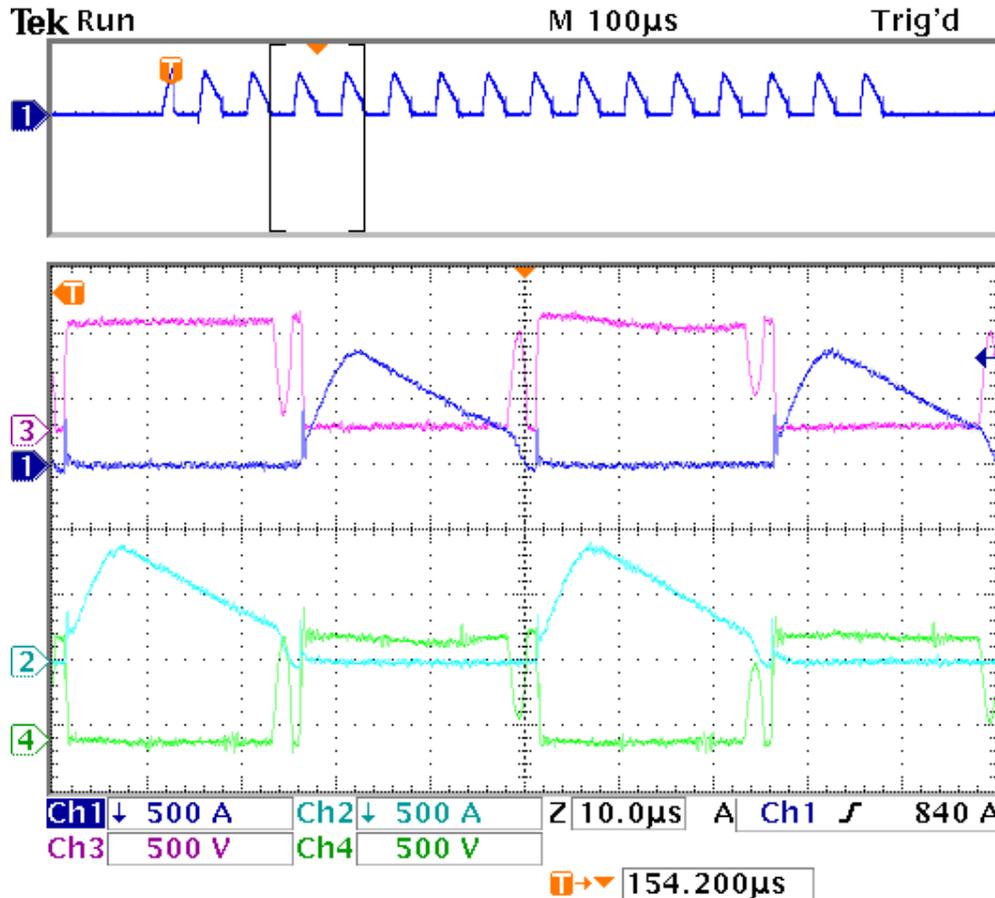
First Article ORNL Driver

Modulator Droop Problem



- Example of SCL-Mod1 Output Voltage Waveform
- ~8.3% droop over 1.35 ms pulse width
- RF power reduction at end of pulse

Pulse Droop Compensation

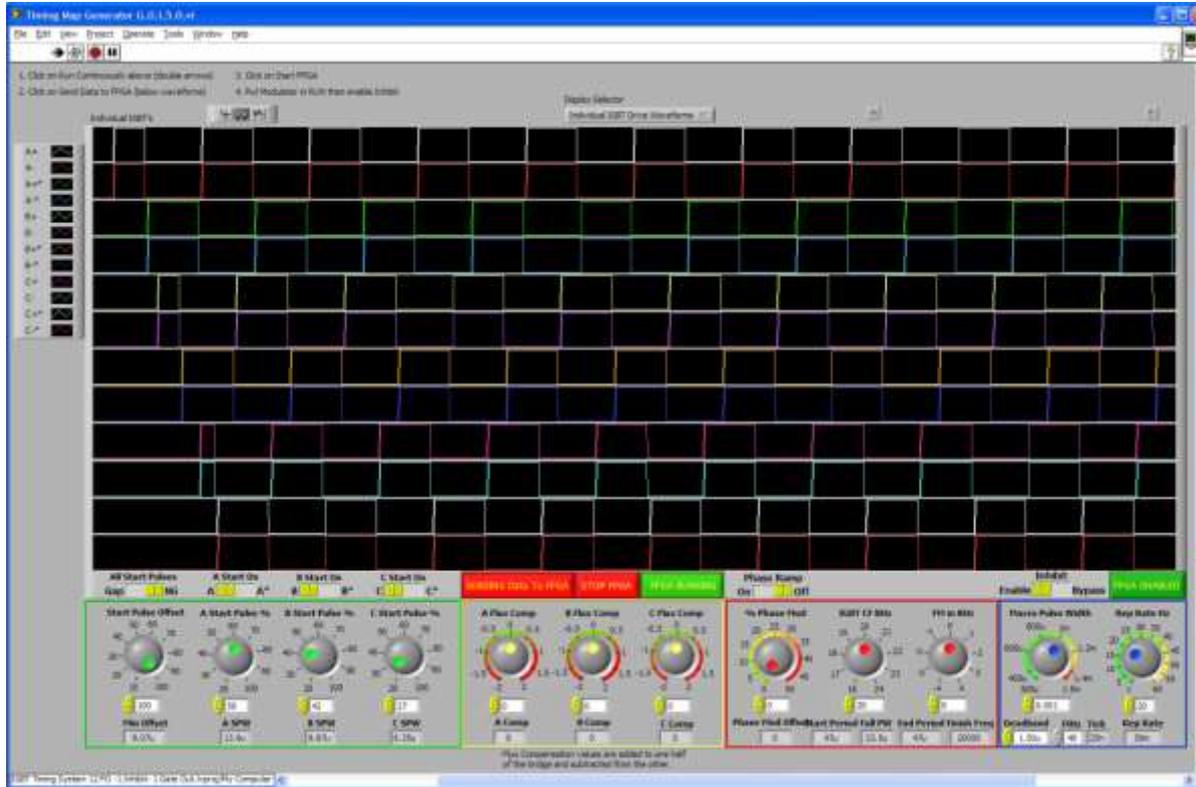


69 kV
“phased
back” –
PWM
doesn’t
work

16 Apr 2004
14:46:51

- Turn-off switching losses too high in initial tests
- Oscillations with device capacitance make constant dead band desirable

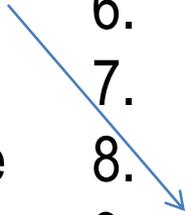
New Controller Development



- LabView / FPGA based development system for IGBT timing pulses
- Start pulse adjustment capability
- Flux Compensation feature
- Phase shift & frequency adjustment capabilities
- Presently characterizing IGBT performance under different conditions

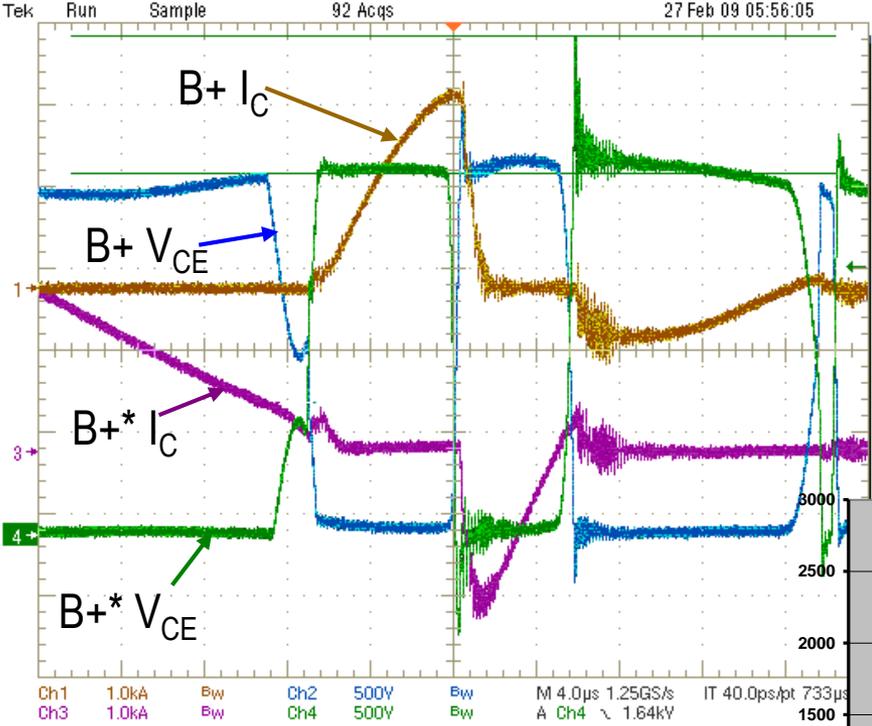
New Controller Functionality & Path Forward

- Integrates several existing chassis & provides additional monitoring, including first fault capture
- Provides data capture, logging, and EPICS retrieval
- With new driver, provides auto. gate timing corrections & monitors IGBTs
- Provides pulse flattening, flux compensation, and drift correction
- Allows for 4 phase operation
- Modular and easily reconfigured
- Interim testing supported with reduced existing controller functionality

1. Freq. & Phase control developed
 2. Develop IGBT fault handling
 3. Develop analog hardware & code
 4. Develop fiber interface
 5. Develop digital I/O interface
 6. Digital firmware
 7. EPICS interface & code
 8. Gate timing firmware
 9. Modulation / feedback code
 10. Integrated testing
- 

Start & Finish Pulse IGBT Stress

File Edit Vertical Horiz/Acq Trig Display Cursors Measure Masks Math MyScope Utilities Help



Buttons

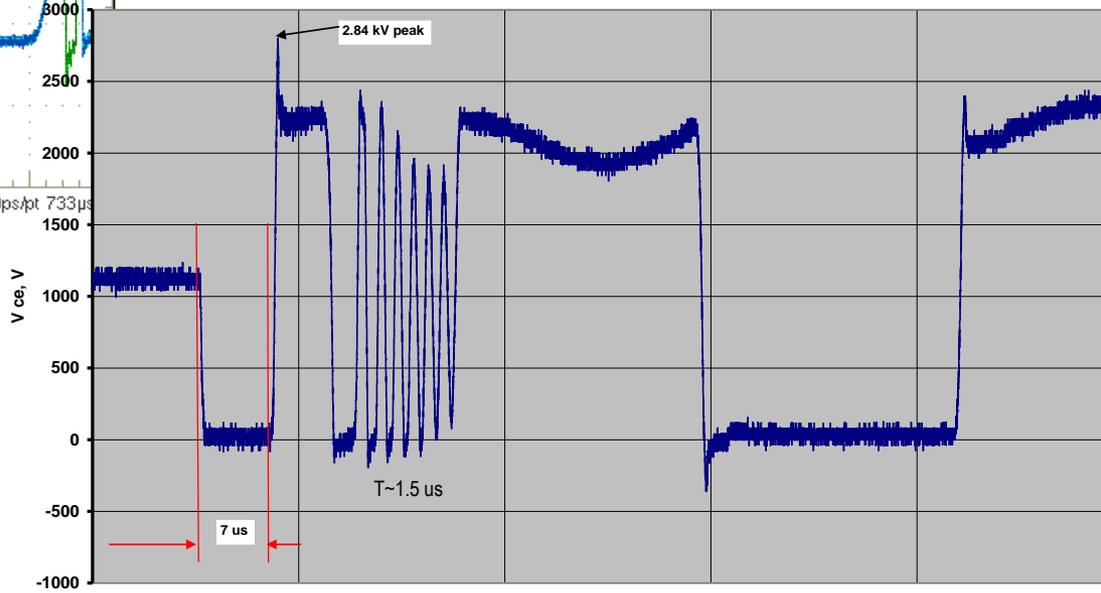
Curs1 Pos
3.05kV

Curs2 Pos
2.21kV

V1 : 3.05kV
V2 : 2.21kV
ΔV : -840.0V

DTL-1 Mod
"A+" phase, Voltage across IGBT (first pulses)
V mod = 115 kV

04.27.09

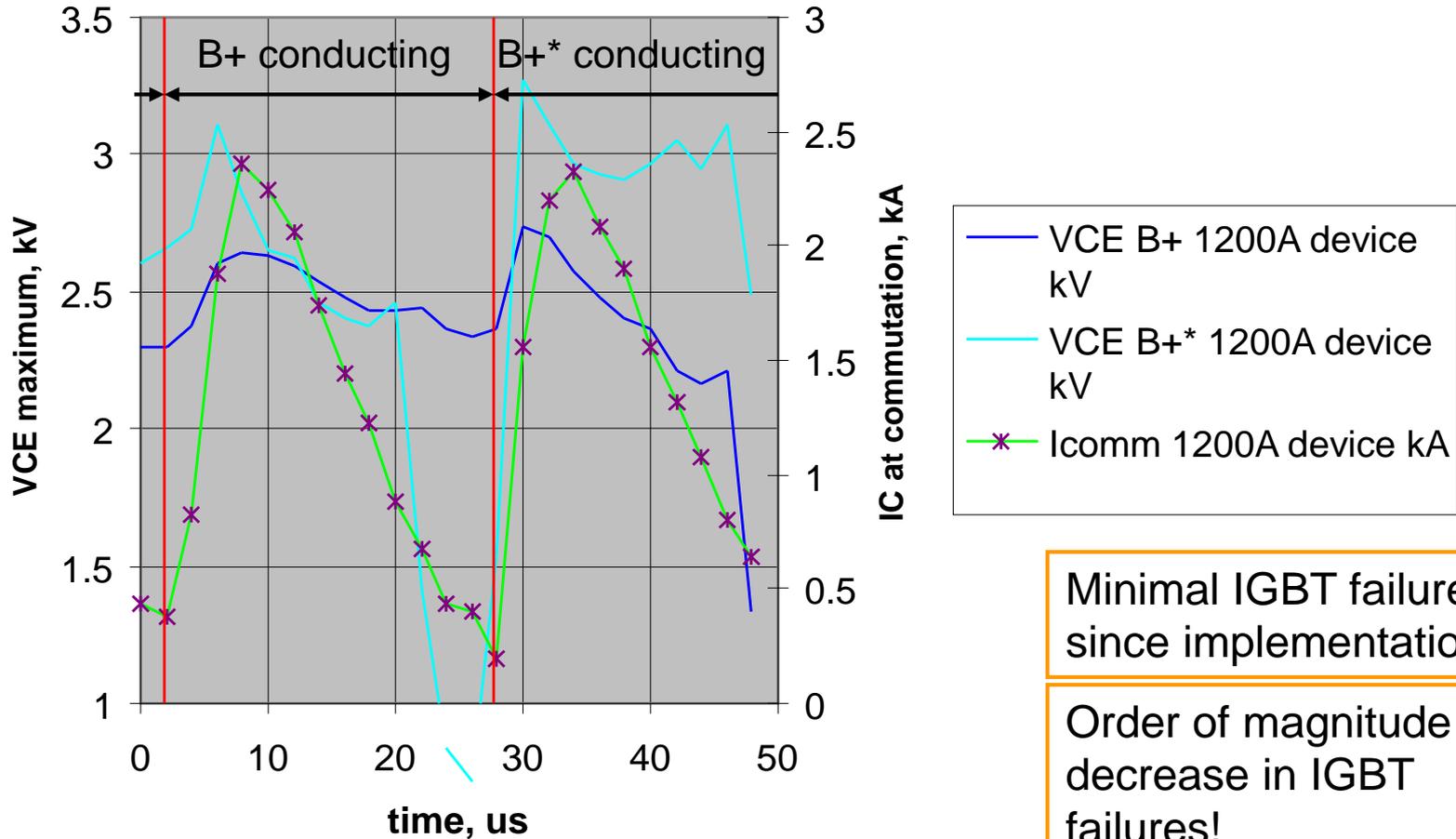


Time
20 us/div



End of Pulse Over Voltage

End of Pulse 1200A IGBT Characteristics



Minimal IGBT failures since implementation!

Order of magnitude decrease in IGBT failures!

In-tank Component Reliability

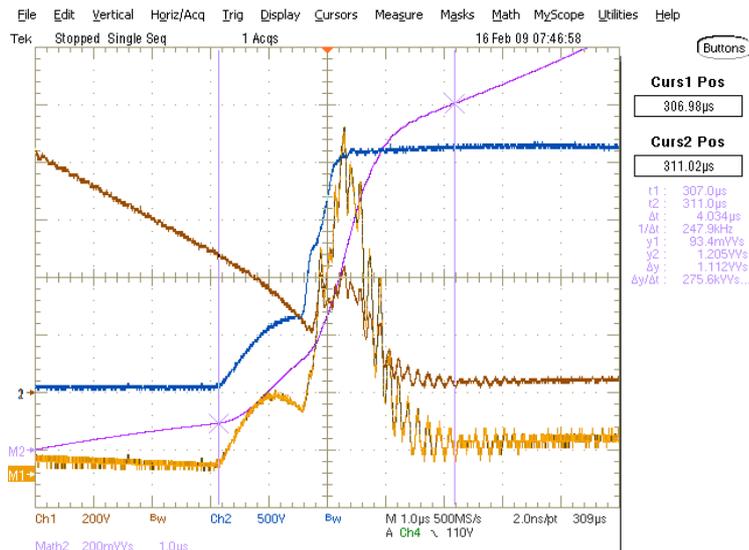
- Study of in-tank components revealed that several did not possess proper engineering de-ratings
 - Capacitors – dissipation factor resulted in thermal failure – estimated ~200 W dissipation, 100°C
 - De-Qing resistor – operating power exceeds rating
 - Divider capacitors – inadequate voltage rating
 - Connecting wires/cables – high current density
- Analysis based on PSpice simulations & device datasheets
- Redesign/replacement process started
- Test capacitors ordered from vendors, testing planned for thermal performance
- Major effort planned for upcoming Summer shutdown



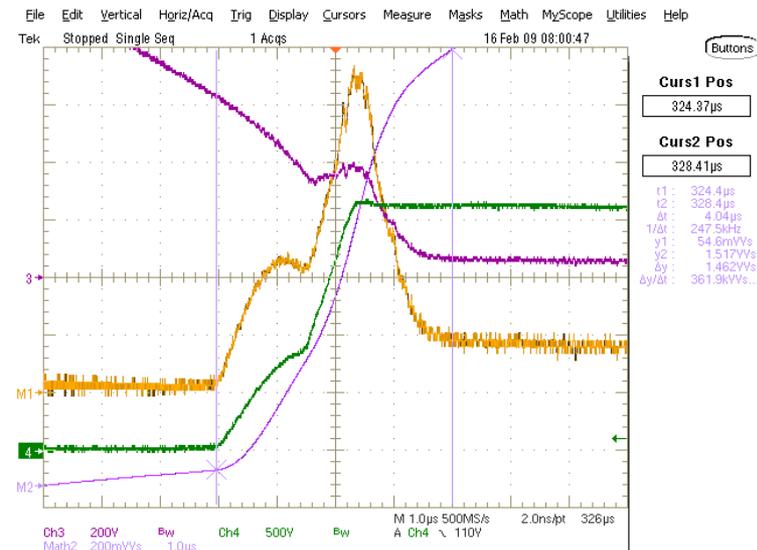
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IGBT Alternate Solutions

- Existing 3300 V, 1500 A devices (Eupec/Mitsubishi)
 - ~30% higher switching losses, mainly at turn-off
 - Longer current tails at turn-off
 - Increased losses likely offset any reliability gains from higher current rating...
- Mitsubishi CM1200HG-90R 4500 V / 1200 A power module
- Westcode Press Pack 4500 V / 1200 A IGBT
- ...more to come...

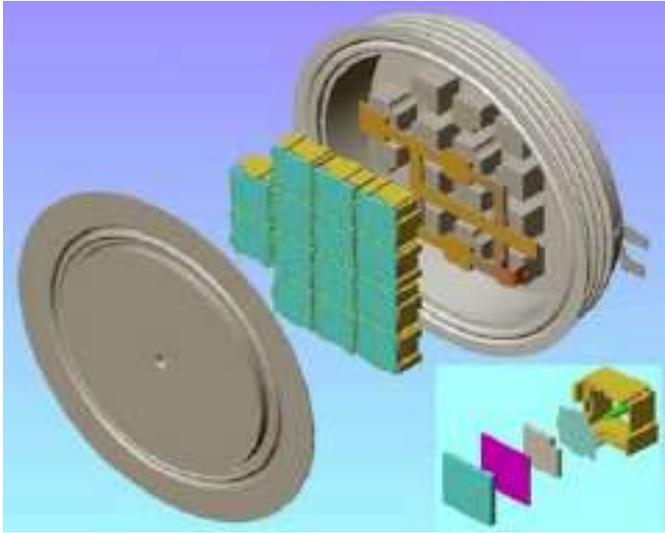


Eupec 1200 A



Eupec 1500 A

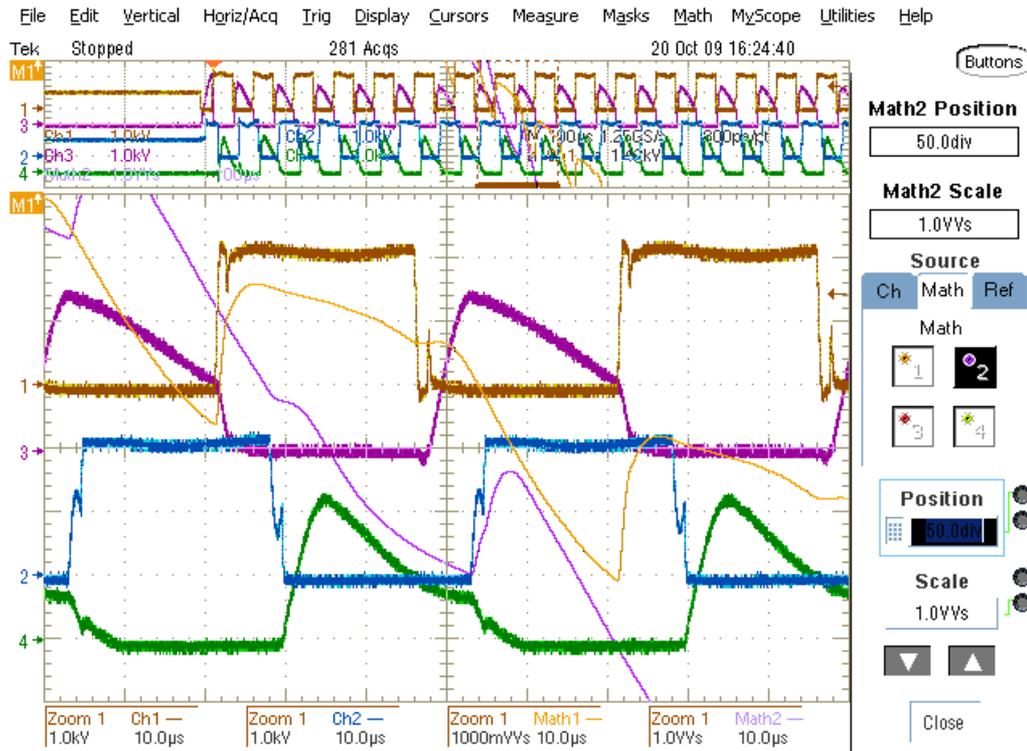
Next Generation IGBTs



Next-generation Press-Pac IGBT devices

- Higher voltage rating (4500 vs. 3300 V), higher current rated recently available
- External anti-parallel diode required
- Developed and peak power tested at SLAC and in testing at ORNL
- Under consideration for MTBF on RFQ HVCM, higher operating voltages on SCL modulators, ultimately PUP
- ~\$40k semiconductors per modulator + switch plate mods and development costs

Initial Performance Comparison of 4500 V IGBTs



Calorimetry results (± 1100 V, 71 kV, 1335 ms, 30 Hz):

Mitsubishi $\langle P \rangle = 2.1$ kW

Westcode $\langle P \rangle = 1.8$ kW

$E_{\text{off, M}} = 2.3$ J, $E_{\text{off, P}} = 1.6$ J

Long tail on Westcode

Ch. 1, 3: Mitsubishi 4500 V IGBT

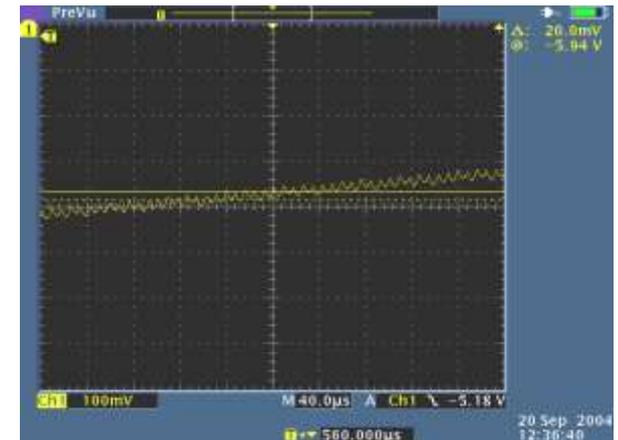
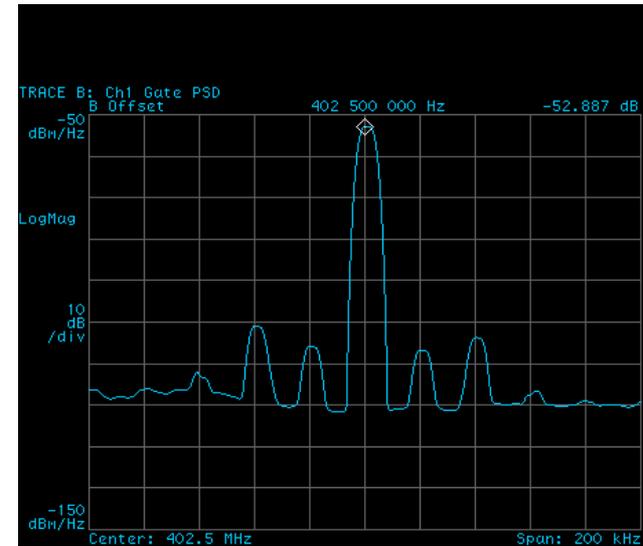
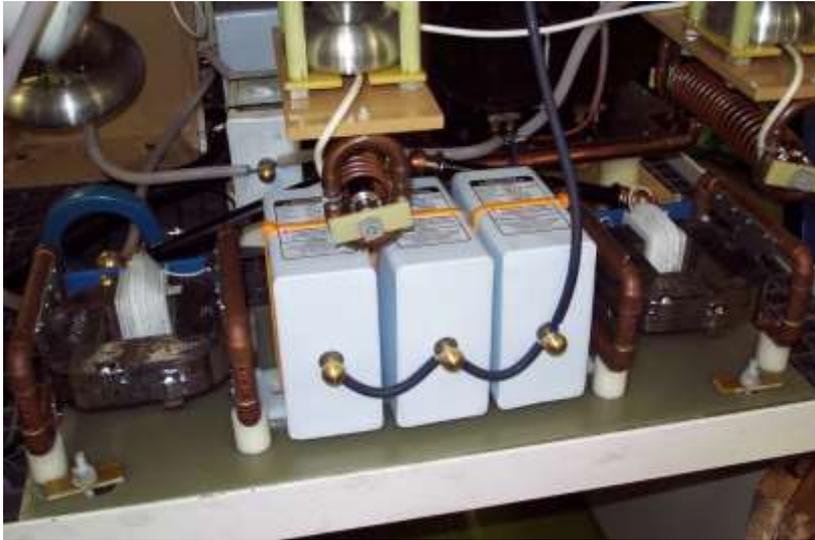
Ch. 2, 4: Westcode 4500 V IGBT

M1: Mitsubishi energy losses

M2: Westcode energy losses

More work needed!

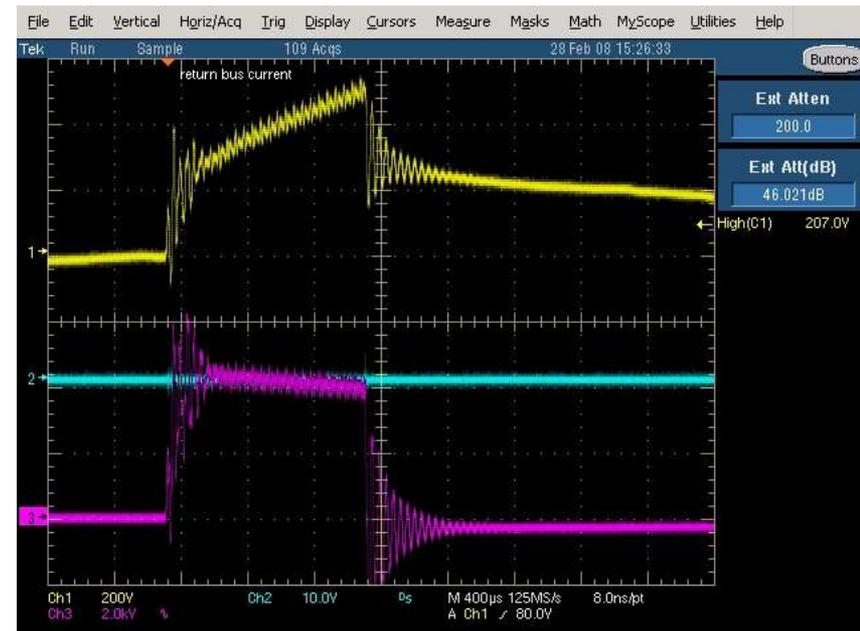
20/40 kHz Harmonic Filter for Ripple Reduction



- 20/40 kHz Harmonic Filters on output section to reduce ripple
 - Factor of 2 improvement in ripple (0.33% p-p)
 - Design exists and tested on a DTL & CCL modulator

Additional Planned Development

1. Main energy storage cap bank fast disconnect switch
 - Minimize fault energy available at switch plate
 - Necessary to support possible redundant H-bridge in the future
 - Instrumentation already in place, developed at SLAC
2. External and redundant oil pumping
 - Eliminates long MTTR in event of water leak
 - Heat exchanger is contaminating DI water system so needs replacing
 - Faulty pump can be rapidly switched out of system and recovered quickly
3. Capacitor bussing improvements to eliminate current ringing
4. Improved IGBT Thermal mgmt.
5. 20/40 kHz Harmonic Traps on modulator outputs

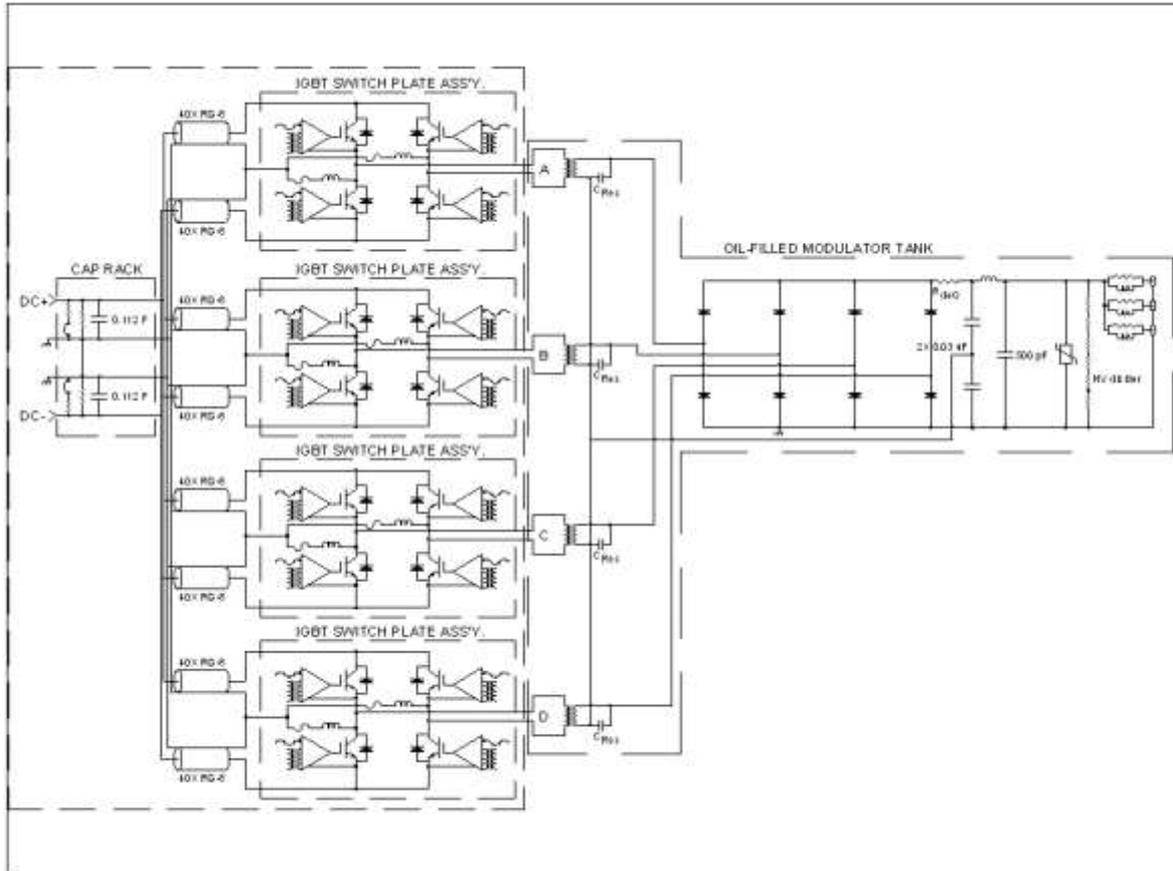


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PUP Implications

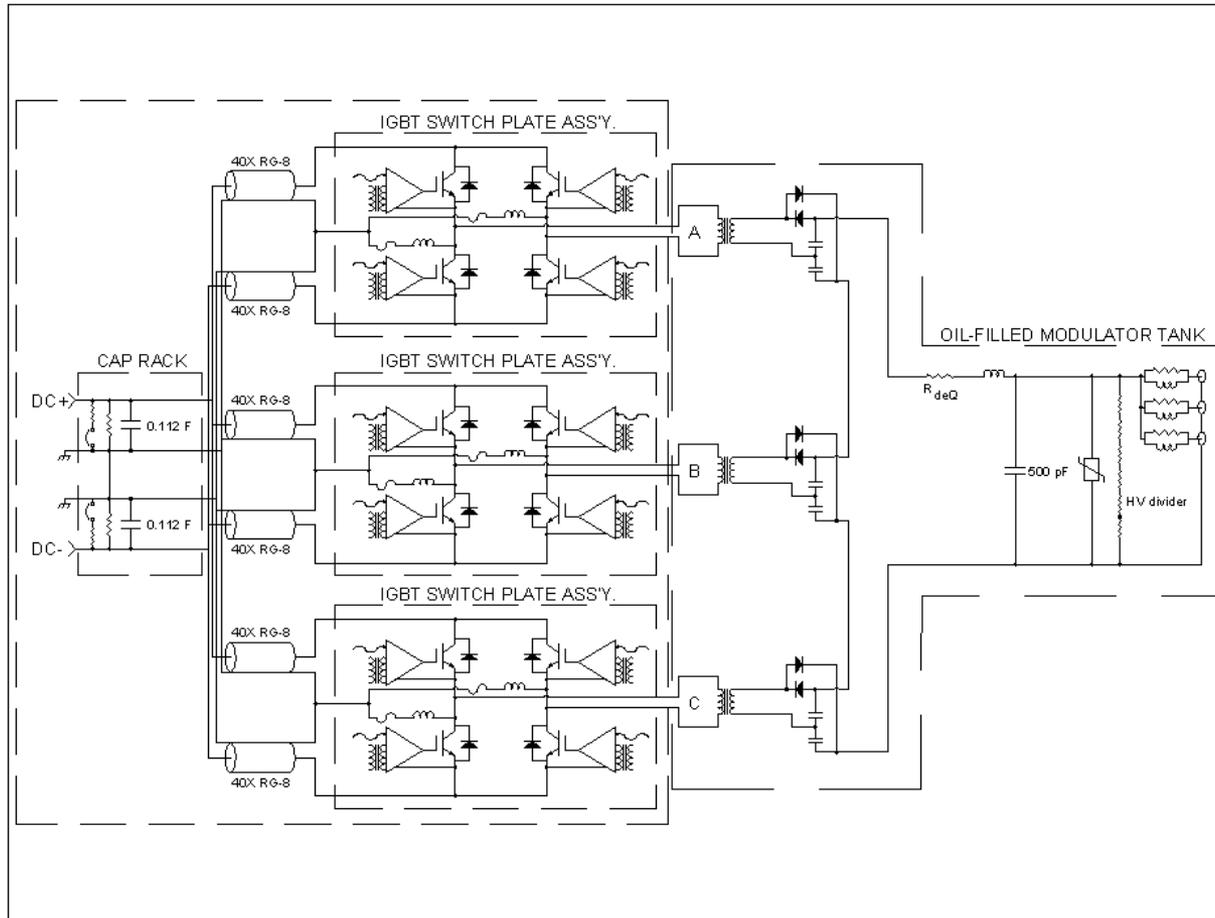
- Desire to run 36 klystrons at up to 700 kW peak (~85 kV modulator output)
- Excess stress on IGBTs of concern, expect MTBF reduction
- 4 modulators / 9-packs helps but possible Second Target Station places additional requirements on modulators
- IGBT improvements may help but compromise reliability gains
- Considering topology modifications
- If successful, mods can be implemented throughout Gallery

4-phase system



- Can achieve true ZCS at turn-off w/ existing components
- Reduces operating voltage levels by about 100 V compared to previous
- New controller design capable of supporting this topology
- Can run w/ 3 phases if switch plate fails

Series-stacked half-bridge system



- Move filter cap after rectifier
- May realize better control of IGBT currents with this topology
- Parallel connection of outputs also viable

Conclusion

- Many subsystems in modulator have been modified and/or replaced
- Early improvements resulted in increased SCR availability
- 60 Hz operation revealed several problems with modulator
 - Over-stressed components
 - Fires
 - Poor overall reliability
- Improvements have helped but still work to do
- Several additional improvements pending