

# Measurements of the 8-Channel Down Converter Module for the New Muon Lab

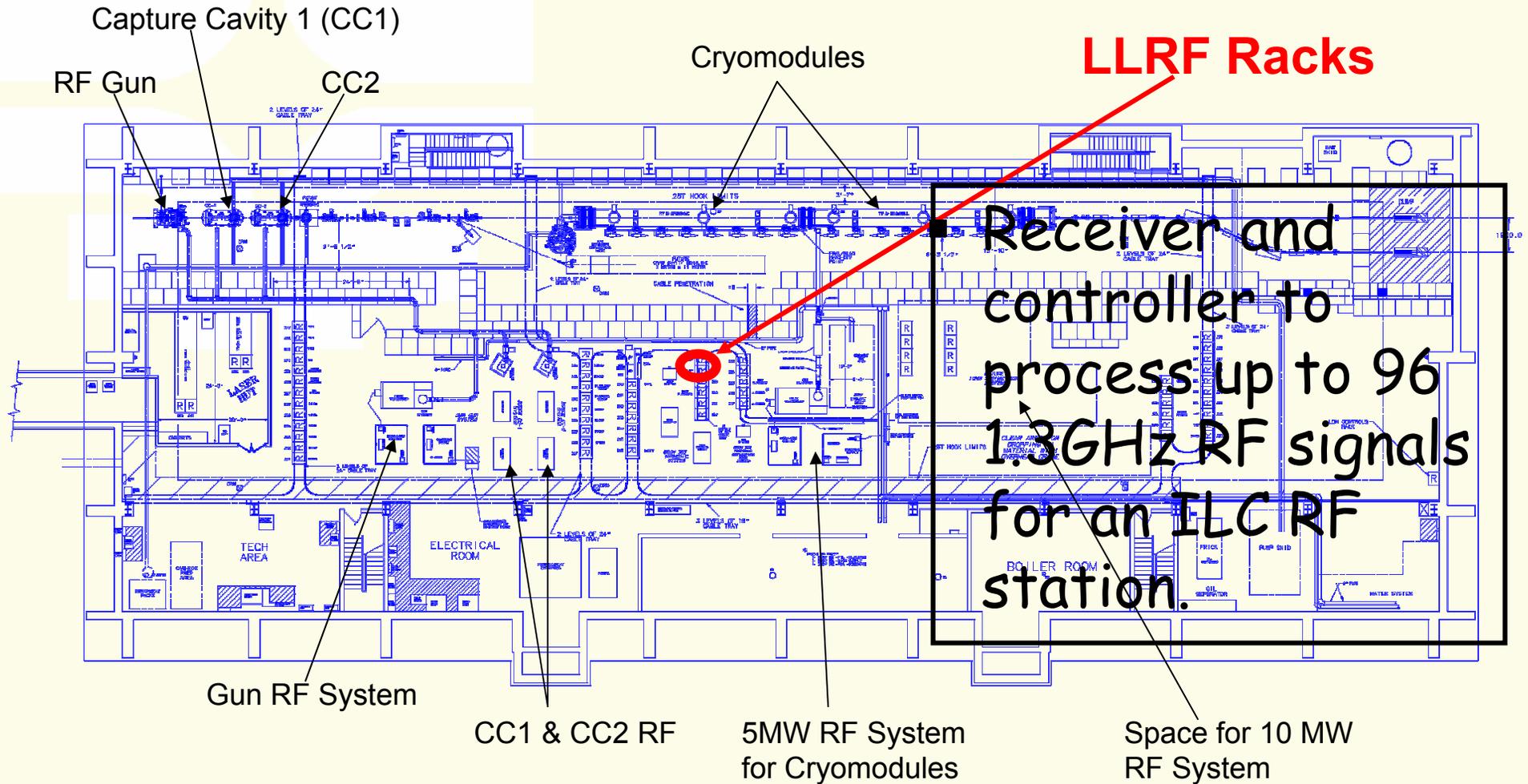


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AD/RF/LLRF

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*LLRF07, Knoxville, Oct. 2007*

# LLRF at NML



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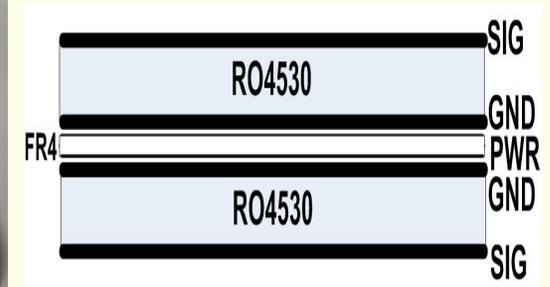
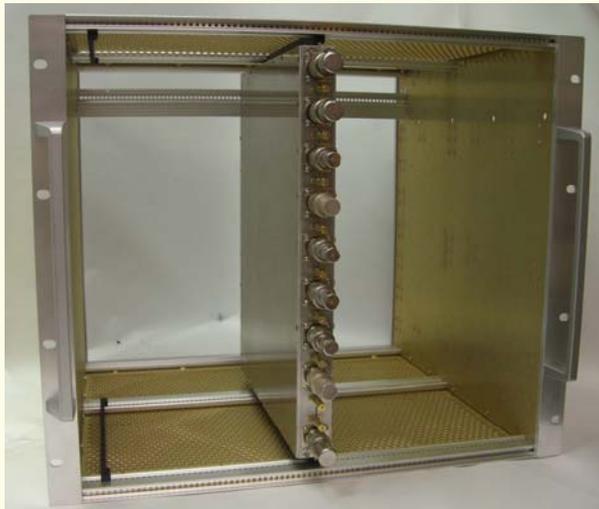
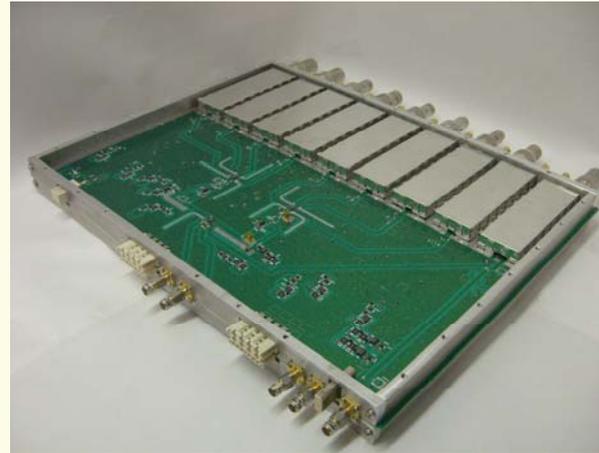


# System Design Goals

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- High channel count
- Low noise
- high linearity
- low crosstalk
- Small connector and cable count
- Reliable, modular, maintainable

# Pictures of the Receiver

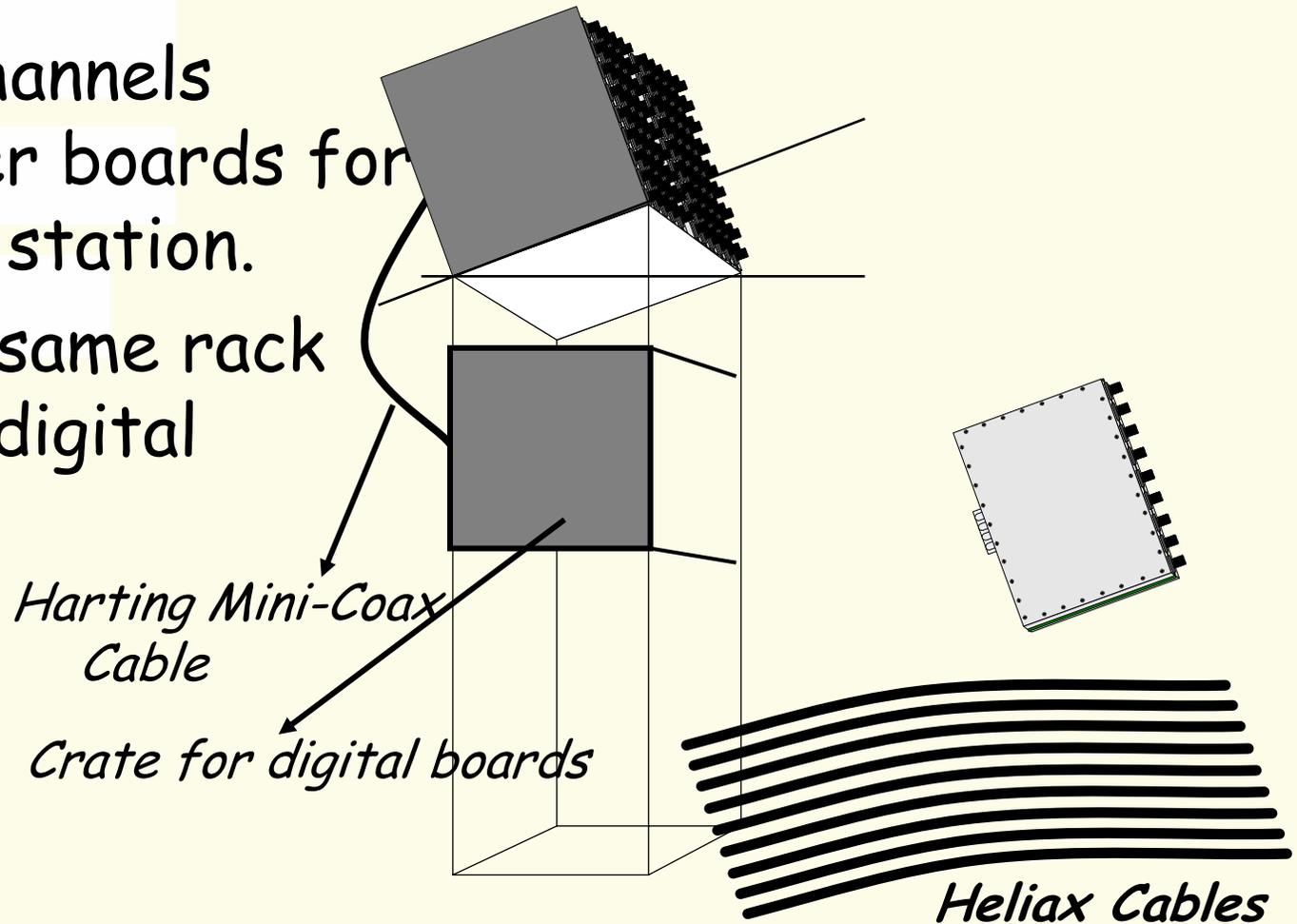


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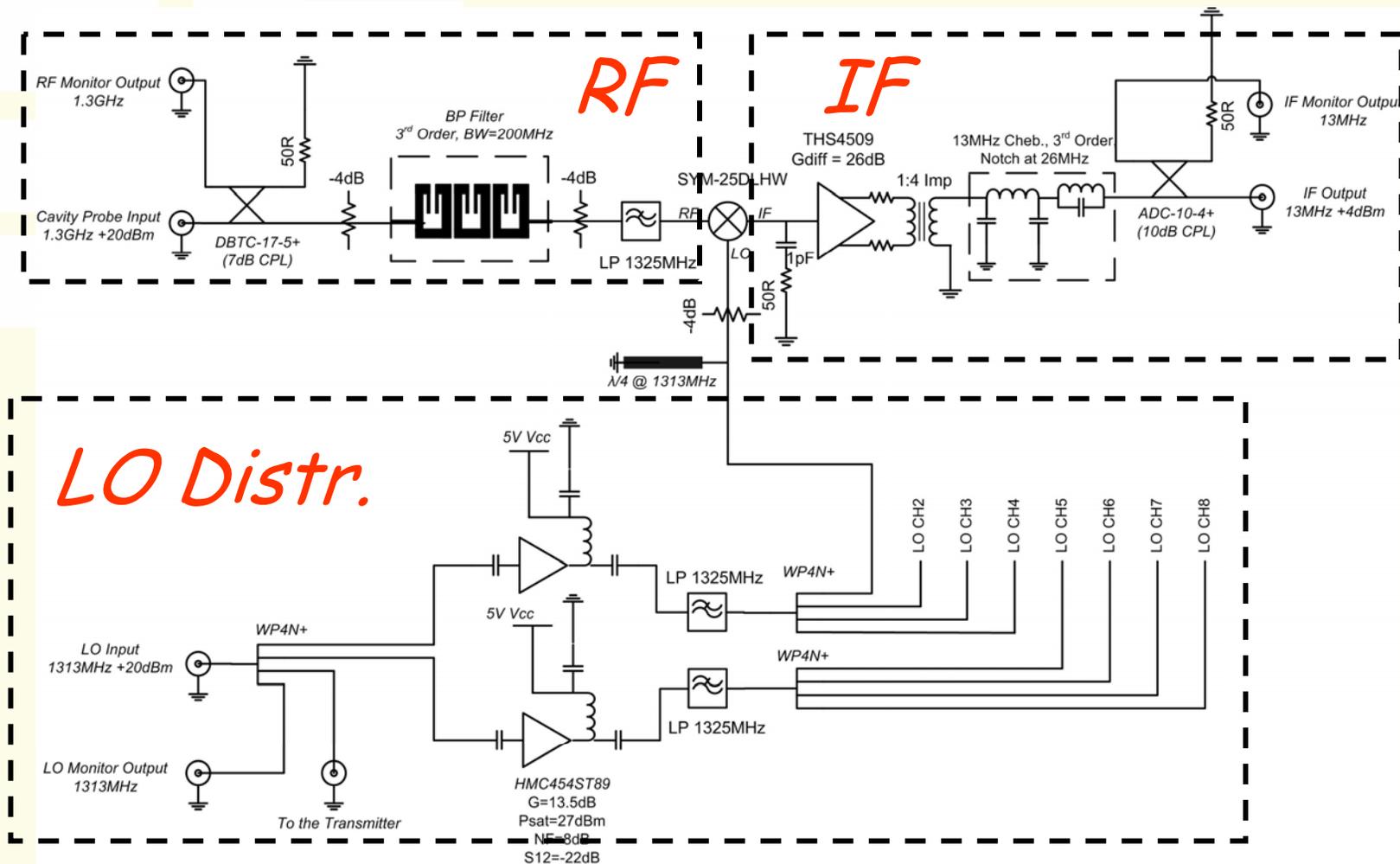


# 96 Channels Receiver

- 12 8-channels receiver boards for one RF station.
- In the same rack as the digital board.



# Schematic of the Rc



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# Architecture Choices

## ▪ Mixers

- Passive vs. Active (low LO power vs. better close-in noise performances)
- LO power vs. linearity
- Single DBM vs. SSB (Simple LO generation vs. good spurs suppression)
- We chose SYM-25DLHW (L13, Pip3=+35dBm, IL=7dB, low close-in phase noise)

## ▪ LO distribution

- 1, 2 or 8 amplifiers
  - *Crosstalk*
  - *Size and power of amplifiers*
  - *Cost*
  - *Matching*
- 2 amps was best for all factors

# Architecture Choices (Cont'd)

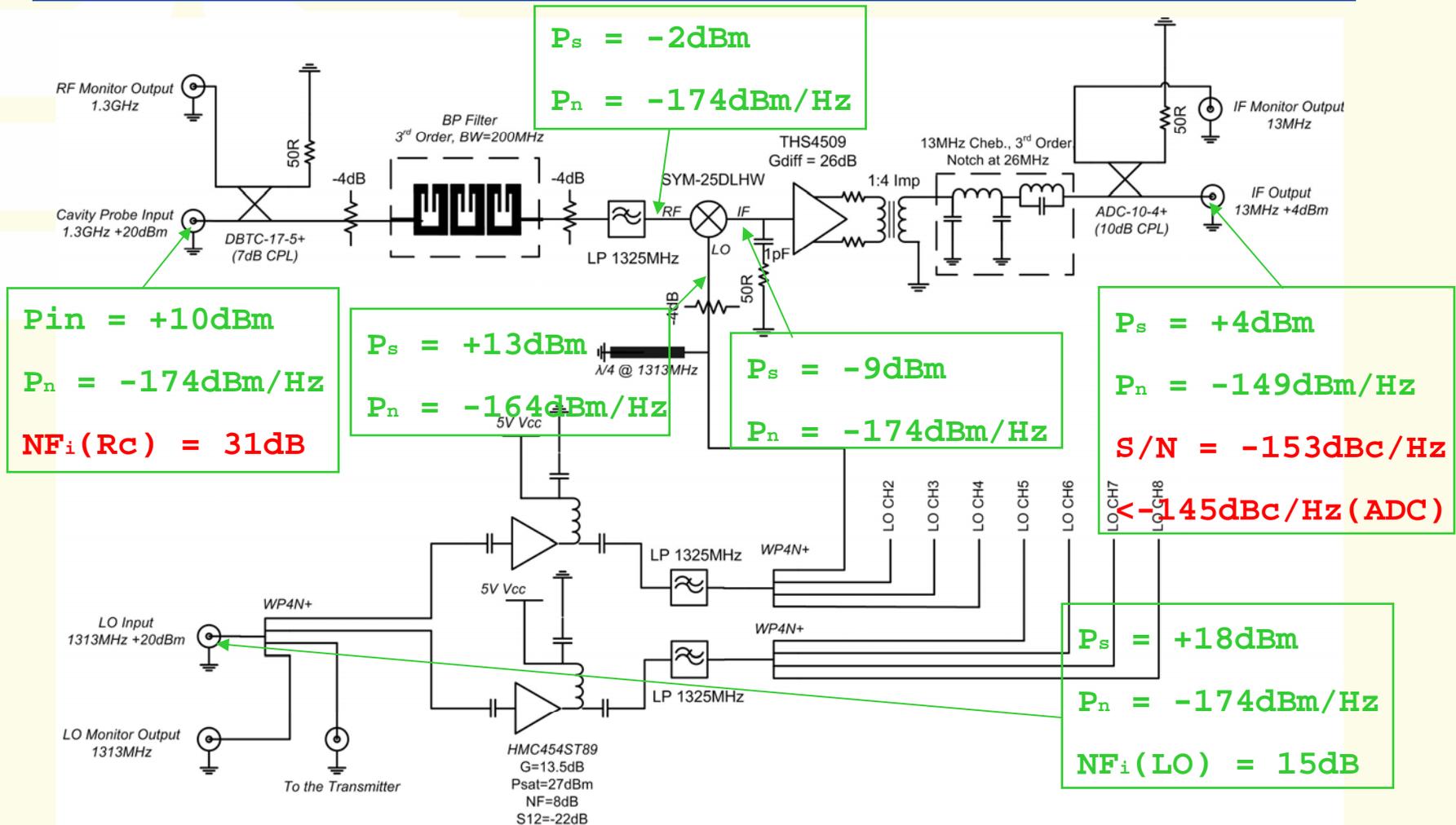
- IF amplifier (IF=13MHz)
  - VGA (e.g. AD833x) or Op-amp
    - *Do we need variable gain?*
    - *Noise should not be dominated by the IF amp*
    - *Good linearity*
    - *50 ohm system at the input and output (additional losses)*

# Measurements

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- Amplitude noise
- Close-in phase noise
- Linearity
- Cross-talk
- S-parameters of RF, LO, IF sections

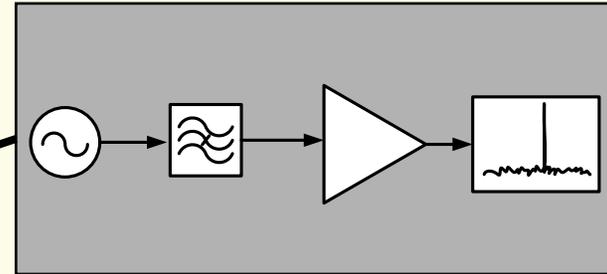
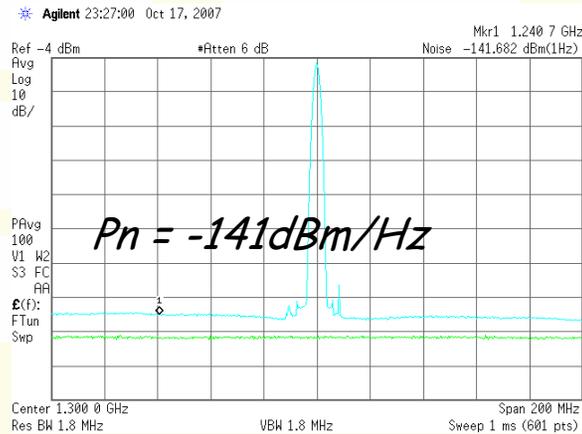
# Signal and Noise Power Levels



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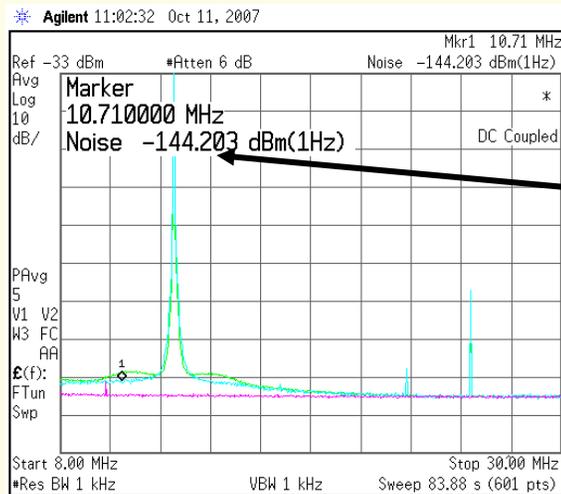


# Amplitude Noise Measurements



$$P_{n\_gen} = -141\text{dBm/Hz} - 27\text{dB} - 1\text{dB}$$

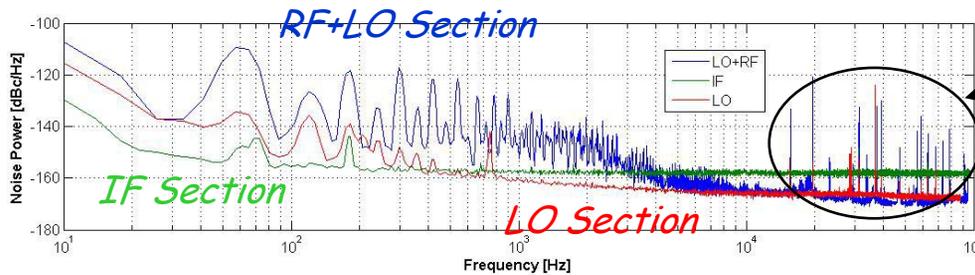
$$= -169\text{dBm/Hz} \text{ (AM Noise from the Source)}$$



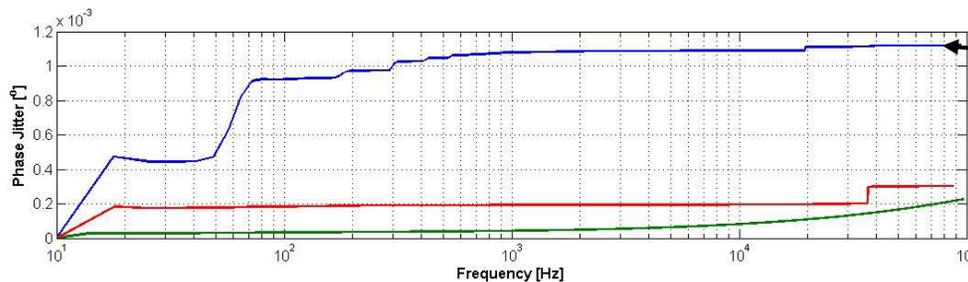
$$P_{n\_Rc\_Out} = -169\text{dBm/Hz} + 31\text{dB} - 6\text{dB}$$

$$= -144\text{dBm/Hz} \text{ (Measured AM Noise at the Output of the Rc)}$$

# Residual Phase Noise Measurements

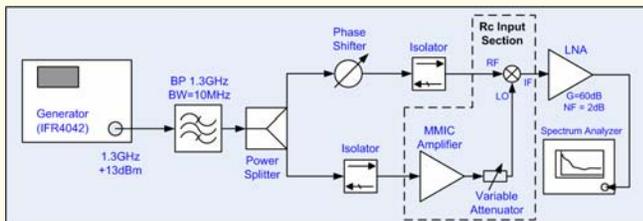


Structure on amplitude (~20kHz)



1e-3°@100kHz  
(similar to what we sampled)

## Measurement Setup



Noise from the aperture jitter of the ADC is not an issue at 13MHz:

$$\text{SNR}@f_s/2 = 20\log_{10}(2\pi 13\text{MHz} \cdot 0.8\text{e-}12\text{s}) = \mathbf{84\text{dB}} \quad (>70\text{dB})$$

Higher IF frequencies? Depends also on the ADC.

# Sampling of the IF Signal

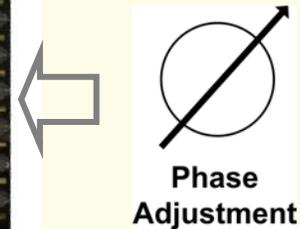
## Multi-Channel Field Control Module



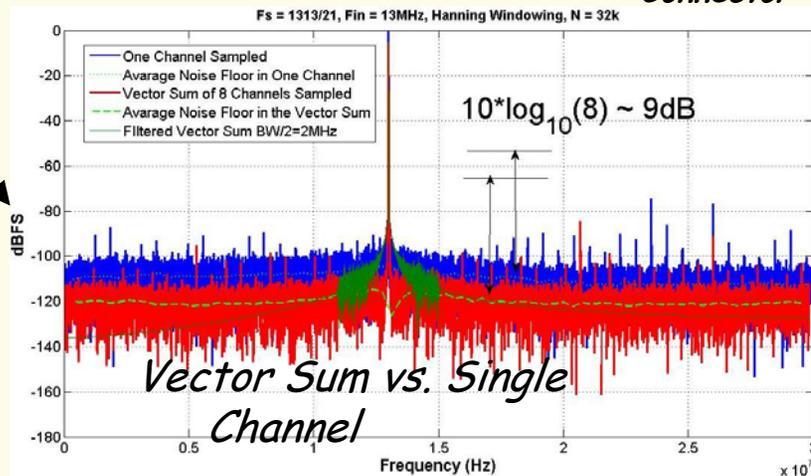
Harting IF Mini-coax

Connector

## 8 Channel Rc



Phase Adjustment



### Measured SNR for one channel

(12bit ADC):

$$\text{SNR}@f_s/2 = 112\text{dB} - 10\log_{10}(32\text{k}/2) = 70\text{dB}$$

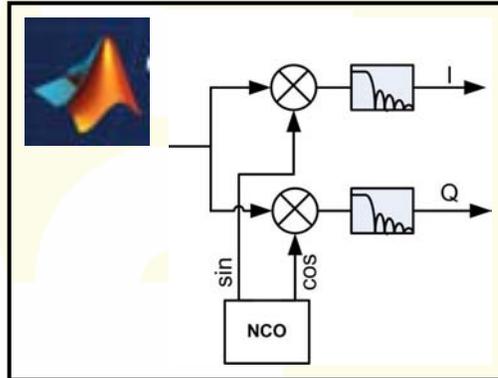
Measured SNR for vector sum

(8x12bit ADC):

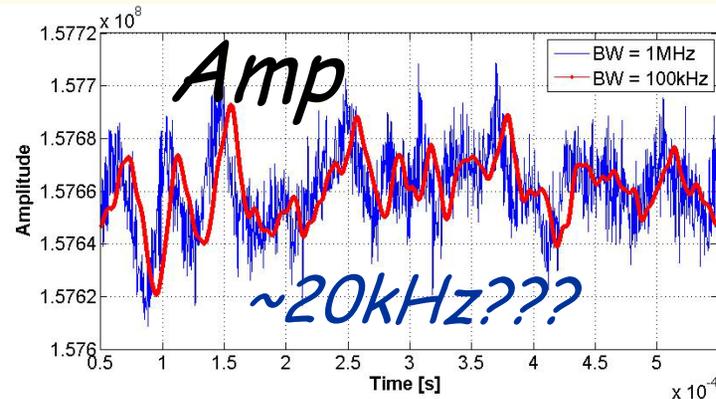
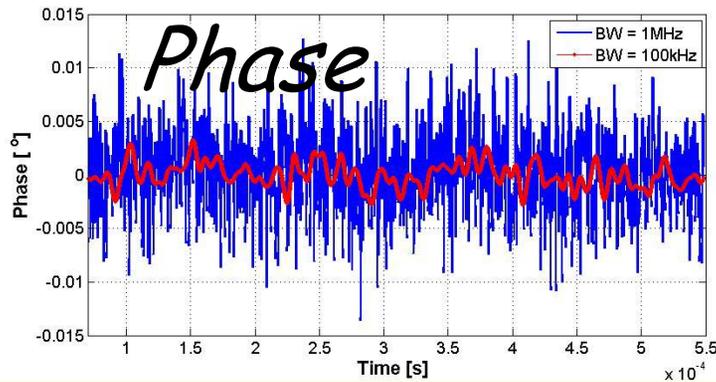
$$\text{SNR}@f_s/2 + 10\log_{10}(8) = 79\text{dB}$$

The SNR -154dBc/Hz (0.002% BW:1MHz) is expected.

# Sampling of the IF Signal Cont'd



$BW = 1\text{MHz}, 100\text{kHz}$



$$\sigma(100\text{kHz}) = 1.1e-3^\circ$$

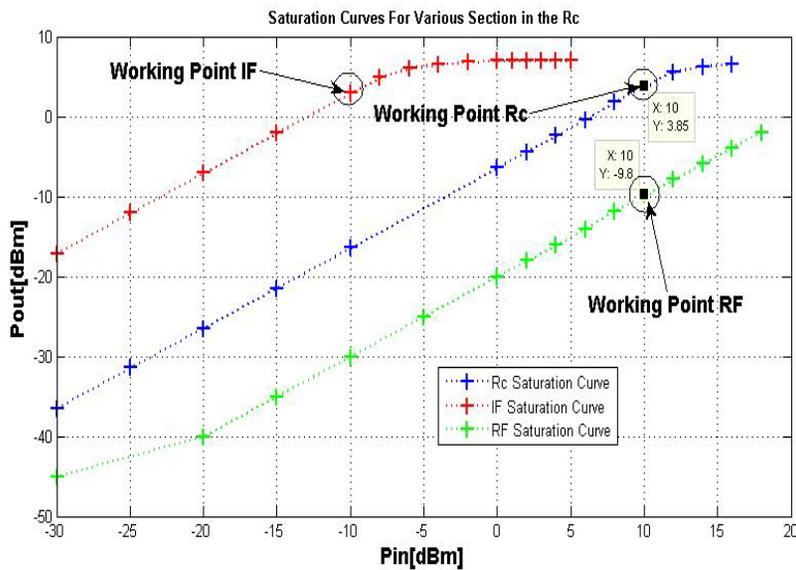
$$\sigma(1\text{MHz}) = 3.7e-3^\circ$$

$$\sigma(100\text{kHz}) = 0.008\%$$

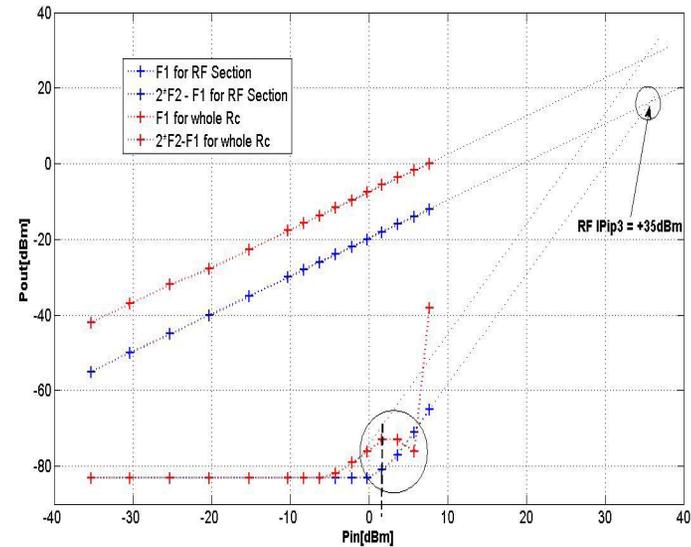
$$\sigma(1\text{MHz}) = 0.01\%$$

# Linearity Measurements

## Saturation Curves for various sections:



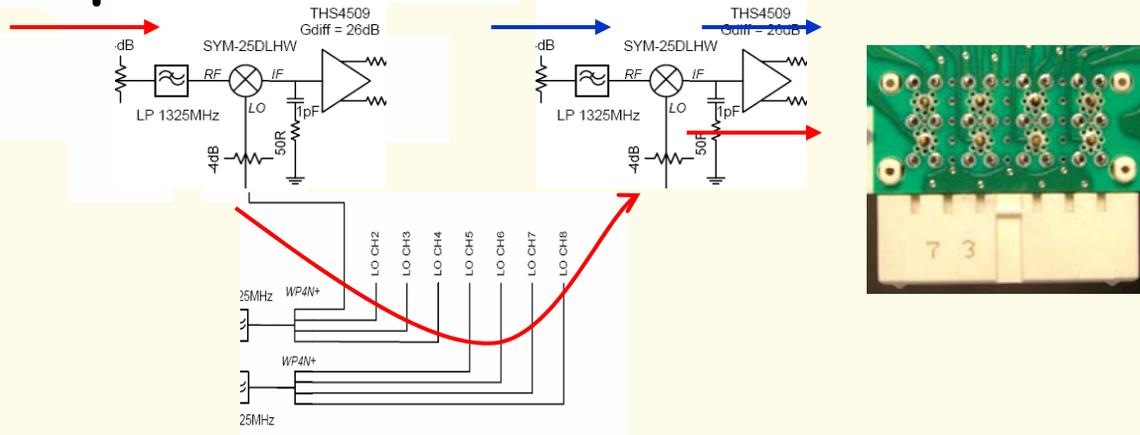
## Two-Tone Test:



*IP3 = +35dBm*

# Coupling Between Channels

- Main coupling through the LO-RF ports of the mixer (SYM-25DLHW).

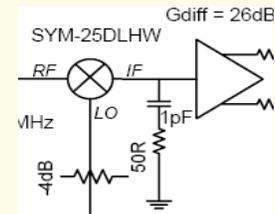


- Other sources : Output connector, improper grounding and shielding.

# Coupling Between Channels Cont'd

## To avoid coupling:

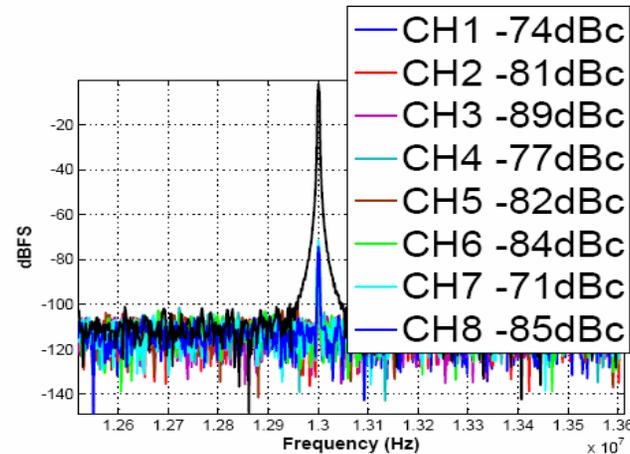
- It is important to achieve broadband matching ( $\sim 2 \times \text{LO}$ ) on all ports of the mixer [1,2].
- *Shielding, stack-up structure, grounding*



# Coupling Measurements

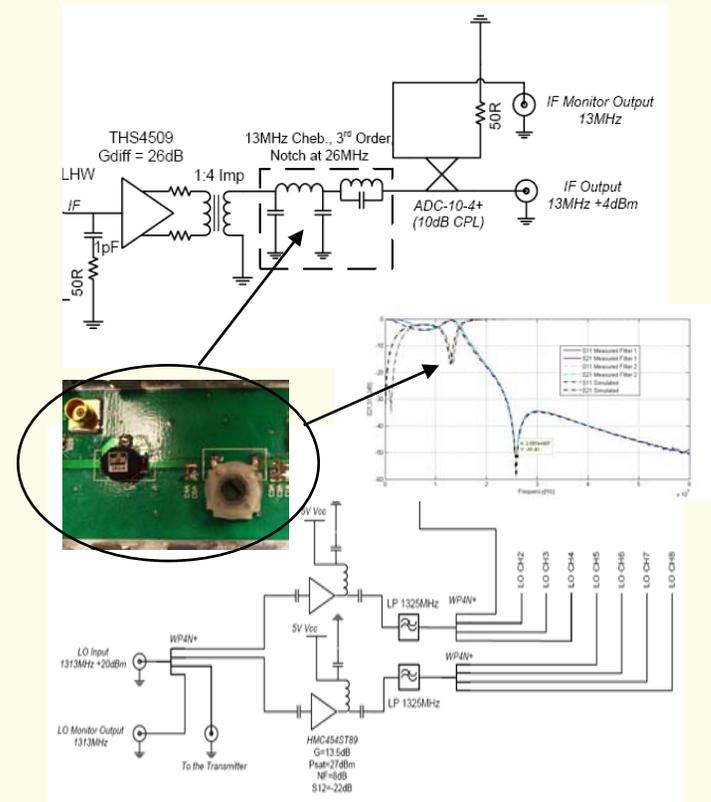
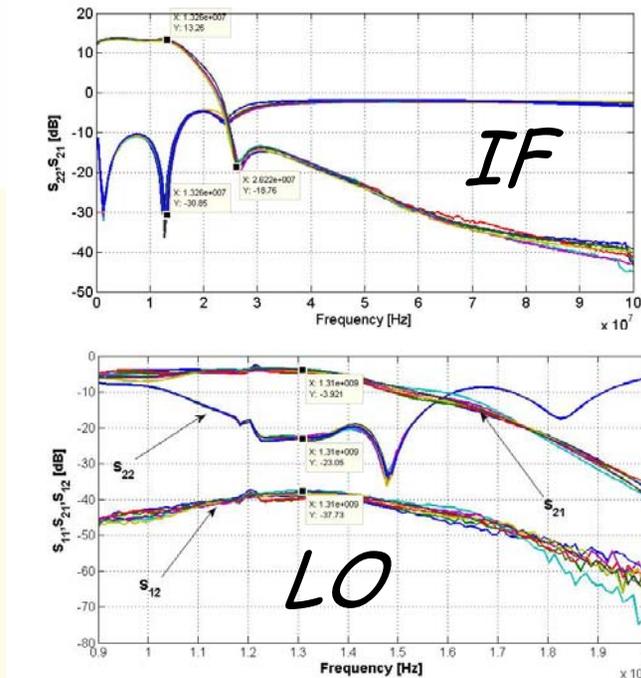
- Coupling Matrix (Single Input - Single Output):
- 7 Channels Input - Single Channel Output (Sampled):

		OUTPUT							
		1	2	3	4	5	6	7	8
INPUT	1	X	-80	-88	-86	-88	-87	-84	-87
	2	-86	X	-87	-83	-88	-88	-89	-87
	3	-87	-83	X	-81	-88	-90	-90	-87
	4	-88	-88	-82	X	-81	-87	-90	-88
	5	-89	-89	-89	-85	X	-80	-89	-88
	6	-89	-89	-90	-87	-80	X	-86	-88
	7	-86	-89	-89	-87	-86	-84	X	-83
	8	-88	-89	-90	-87	-88	-88	-87	X

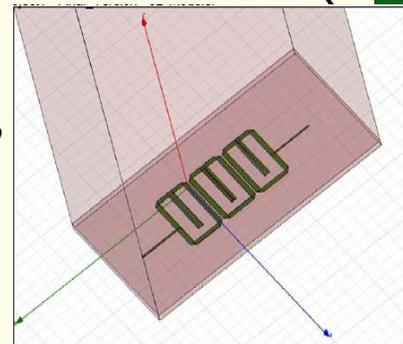
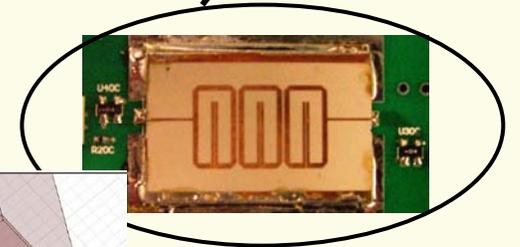
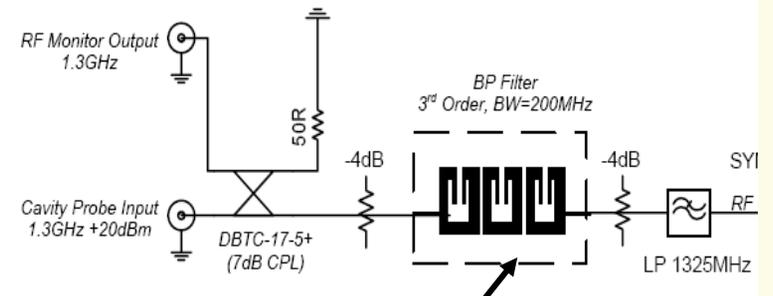
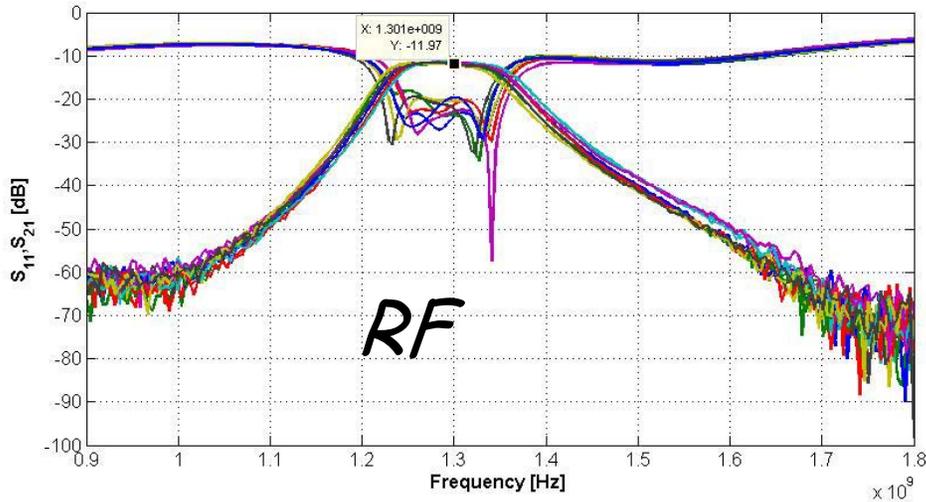


# Transfer Functions

- S Parameters of IF, RF and LO Sections



# Transfer Functions Cont'd



Dispersion Between Channels:

Amp: IF~0.5dB , RF~0.3dB , LO~1.2dB

Phase : IF~40°, RF~33° , LO~200°

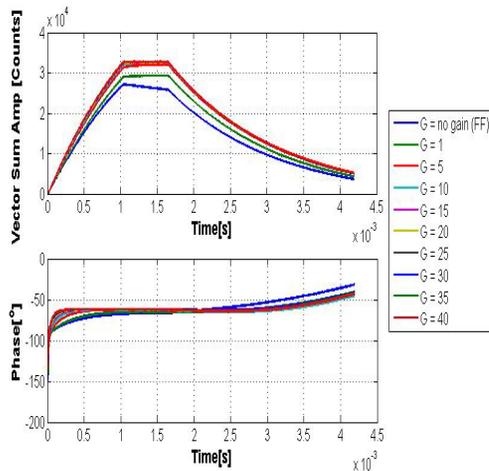
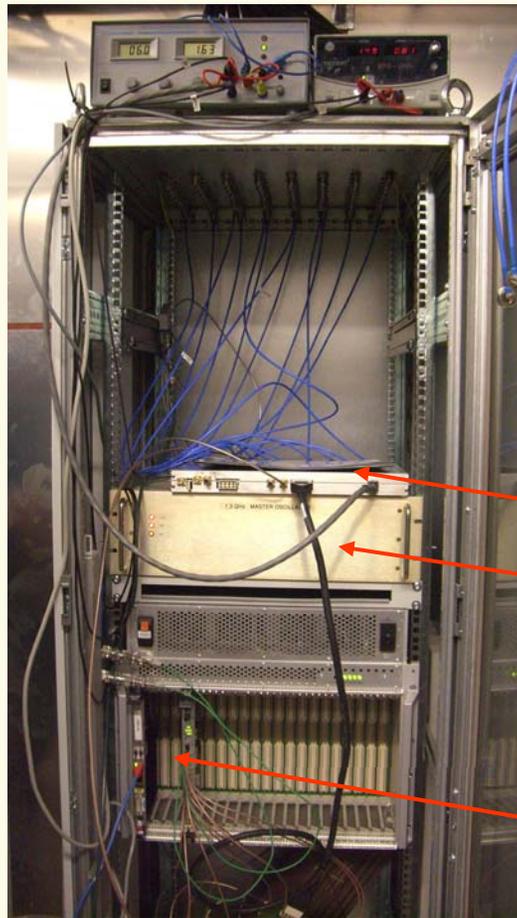
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Fermilab  

# Main Parameters Table

<i>Parameter</i>	<i>Value</i>
<b>Amplitude Noise</b>	31dB (Input Noise Figure)
<b>Residual Phase Noise</b>	$1e-3$ (10-100kHz)
<b>Linearity</b>	+35dBm (Input Pip3)
<b>Cross-Talk</b>	71-90 dB (7 Ch. Connected)
<b>Power Consumption</b>	8W (1A@+6V/0.4A@-6V)
<b>Number of Channels per board</b>	8Rc + 1Tx
<b>Cost/Channel</b>	200\$

# Measurements on ACC1 at DESY



**8 Channel Rc/Tx**

**Master Oscillator**

**LO Generation**

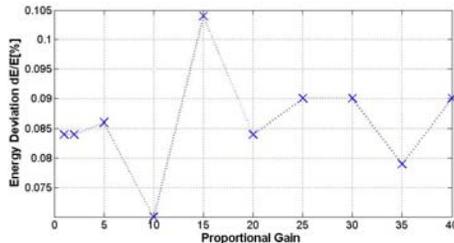
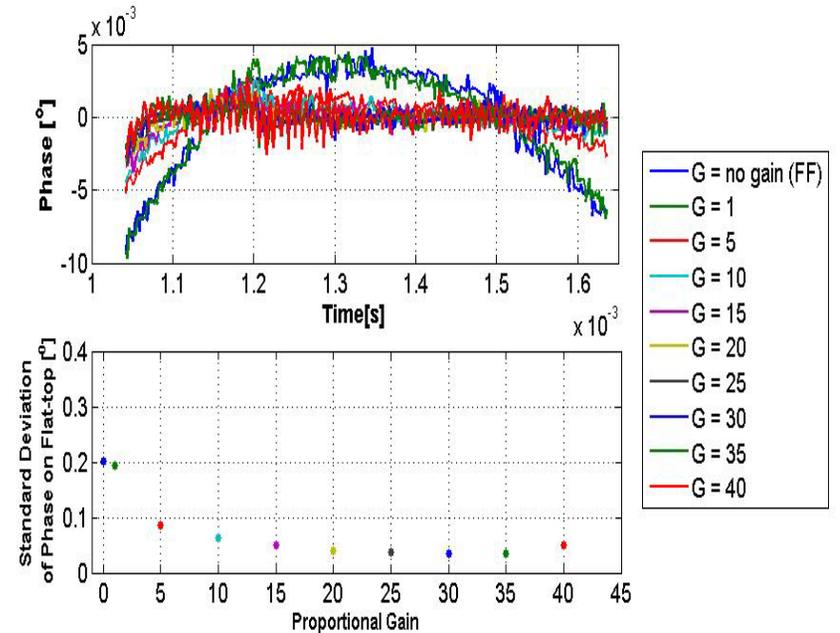
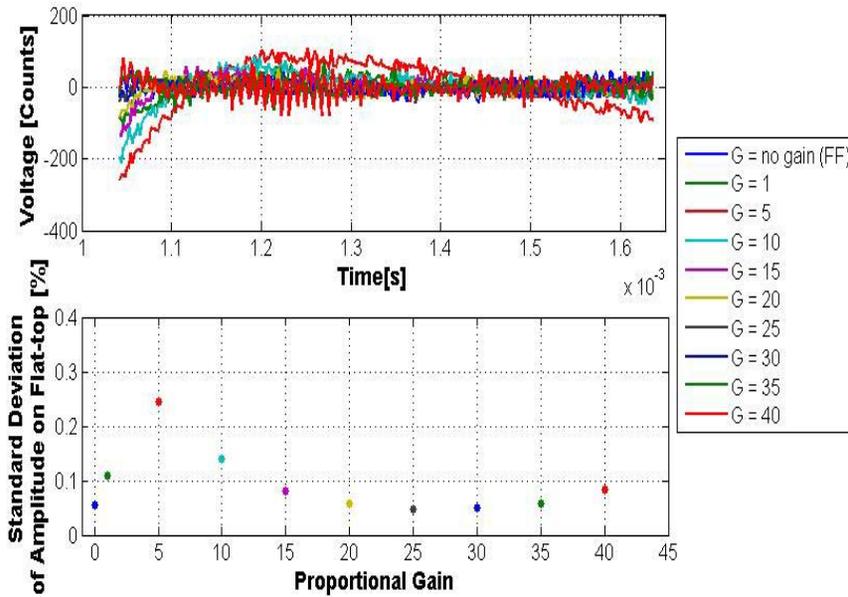
**ESECON**



# Measurements on ACC1 at DESY

*Amp dev. vs. Loop Gain*

*Phase dev. vs. Loop Gain*



*Energy Spread of the beam*



# Acknowledgments

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- AD LLRF Group

- Brian Chase, Ed Cullerton, Julien Branlard, Paul Joireman, Philip Varghese, Dan Klepec, Barry Barnes, Vitali Tupikov

- Thanks to:

- CD LLRF Group (G. Cancelo)
- DESY (F. Ludwig)
- JLab (J. Musson)
- NIST (A. Hati)

# References

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- [1] P. Will, "Reactive Loads - The Big Mixer Menace," *Microwave*, pp. 38-42, April 1971
- [2] M. W. Muterspaugh et al., "Single Balanced Mixer Output Filter," *United States Patent - 5,034,994*, July, 1991

# Backup Slides

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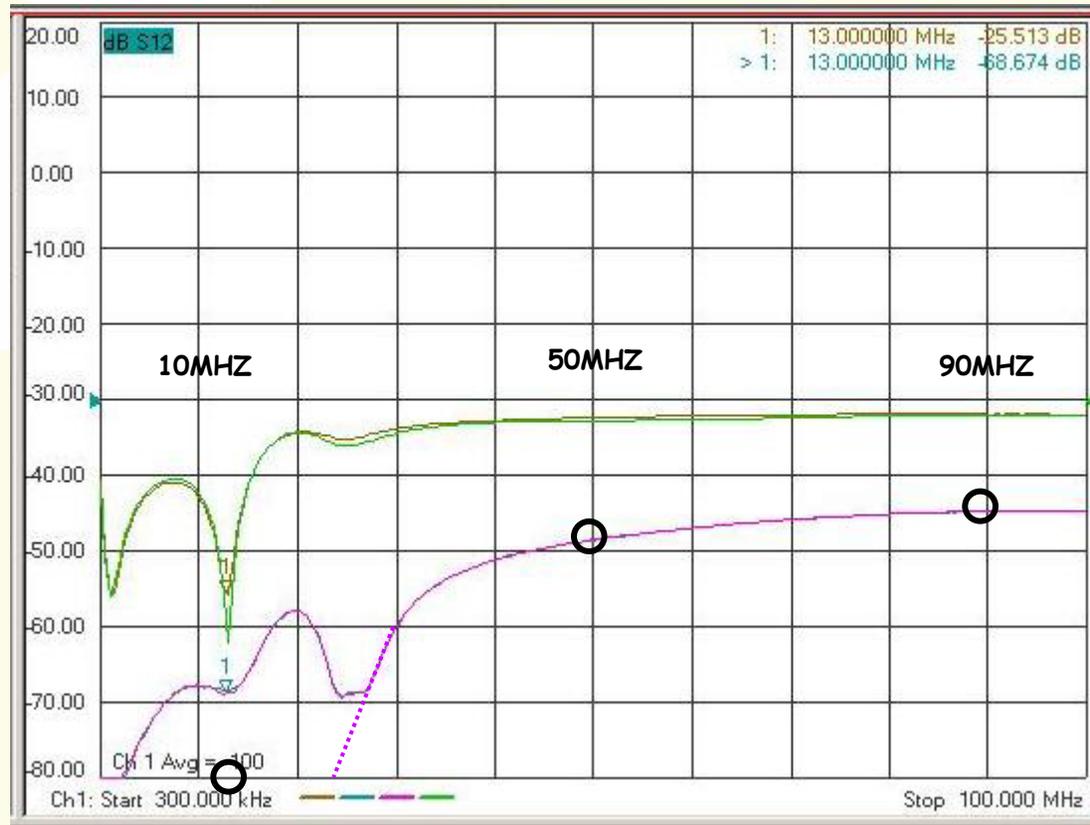


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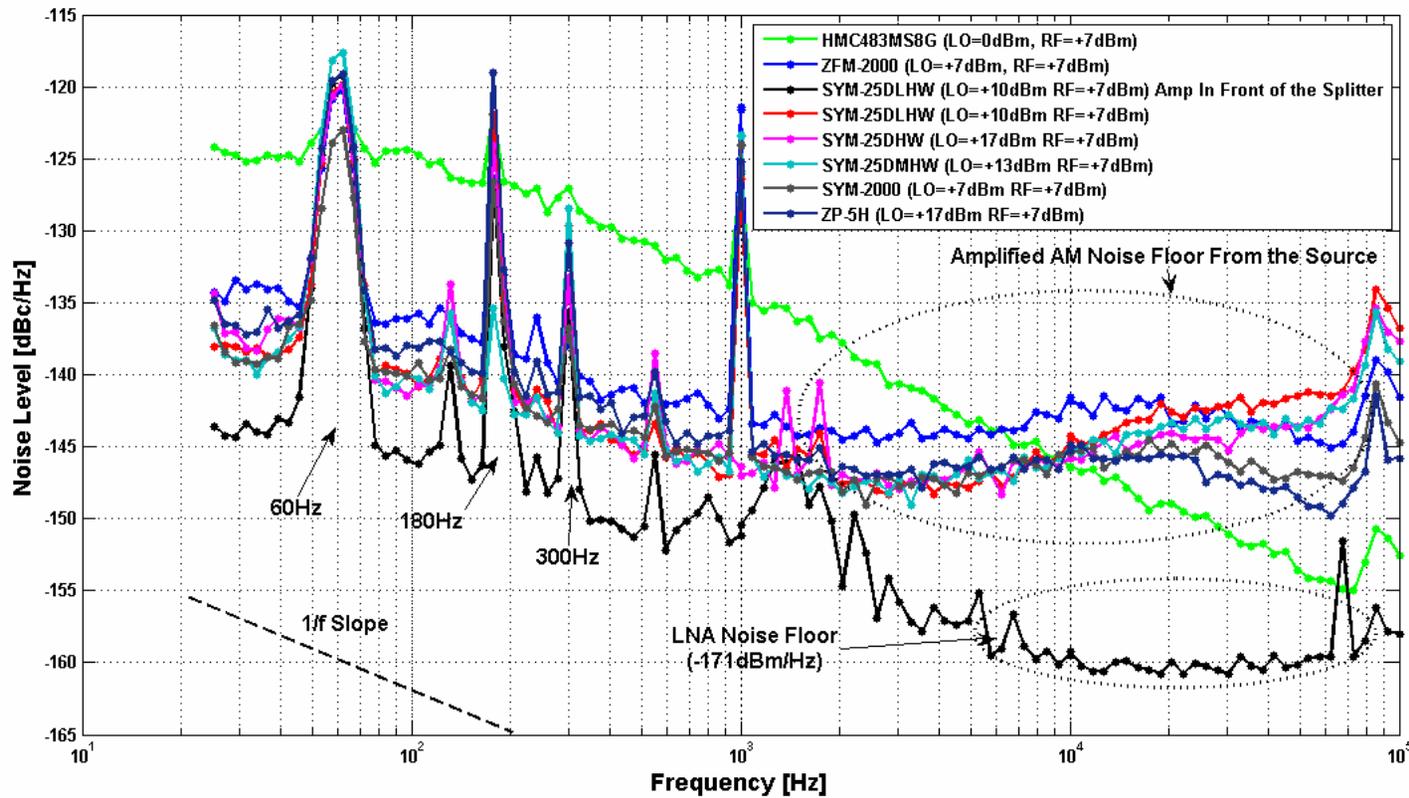
# Coupling vs. Frequency



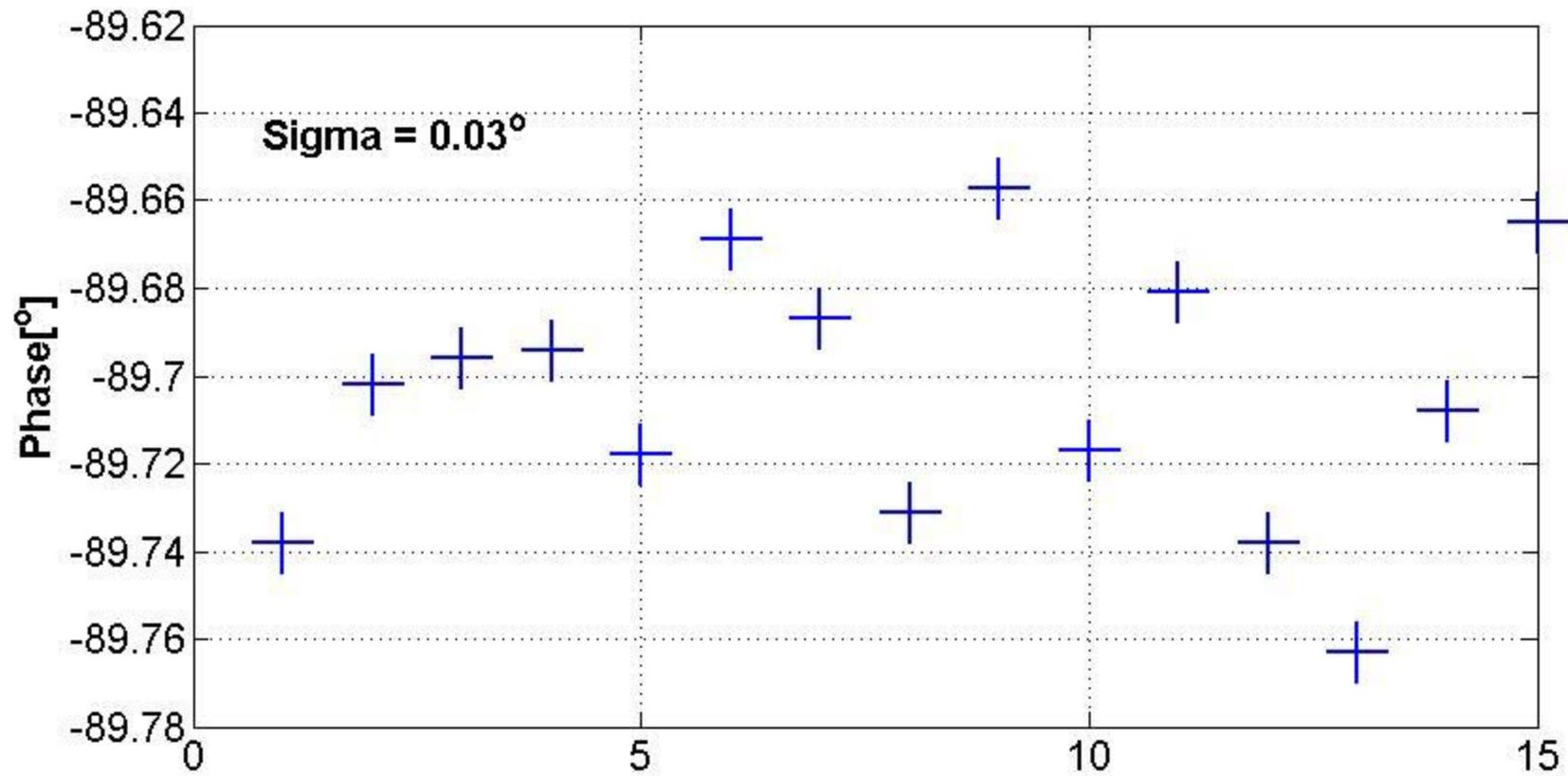
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# Input Stage Residual Phase Noise



# Phase Stability of Harting Mini-Coax Connectors



# Temperature Stability of the Rc

